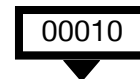


**OTH2021-01351**

**PRELIMINARY HYDROLOGY ANALYSIS  
FOR A-TOWN TRACT 17703**

**LOT 4 – AREA E**



DEPARTMENT OF PUBLIC WORKS  
DEVELOPMENT SERVICES

**APPROVED**

Gabreelle Gonzalez, Assistant Engineer

7/16/2021, 9:52:32 AM

ANAH-OTH2021-01351

Gabreelle Gonzalez

**City of Anaheim  
County of Orange**

**PREPARED FOR:  
LMC  
A LENNAR COMPANY**

**PREPARED BY:  
HUNSAKER & ASSOCIATES IRVINE, INC.  
3 HUGHES  
IRVINE, CA 92618  
(949) 583-1010**

**JUNE 3, 2021**

**W.O. #3916-65**

**PRELIMINARY HYDROLOGY ANALYSIS**  
**FOR A-TOWN TRACT 17703**  
**LOT 4 – AREA E**

**City of Anaheim**  
**County of Orange**



PREPARED UNDER THE SUPERVISION OF:

---

Tu Trinh, R.C.E. 71555

Date

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## **SECTION 1**

## **A. PROJECT LOCATION**

The project site is A-Town, Tract 17703, Lot 4 – Development Area E (DA-E), in the City of Anaheim (City), County of Orange. The site is bounded by an existing gas station on the north, Metro Drive on the west, State College Boulevard on the east, and existing commercial buildings on the south (see attached Vicinity Map for more information).

## **B. STUDY PURPOSE**

This study is to accompany the submittal of a Water Quality report. This study is preliminary, determines the 100-year, 25-year, 10-year, and 2-year peak storm runoff produced from the project site as approved by the City in 2016 for the overall Tract 17703 .

## **C. METHODOLOGY**

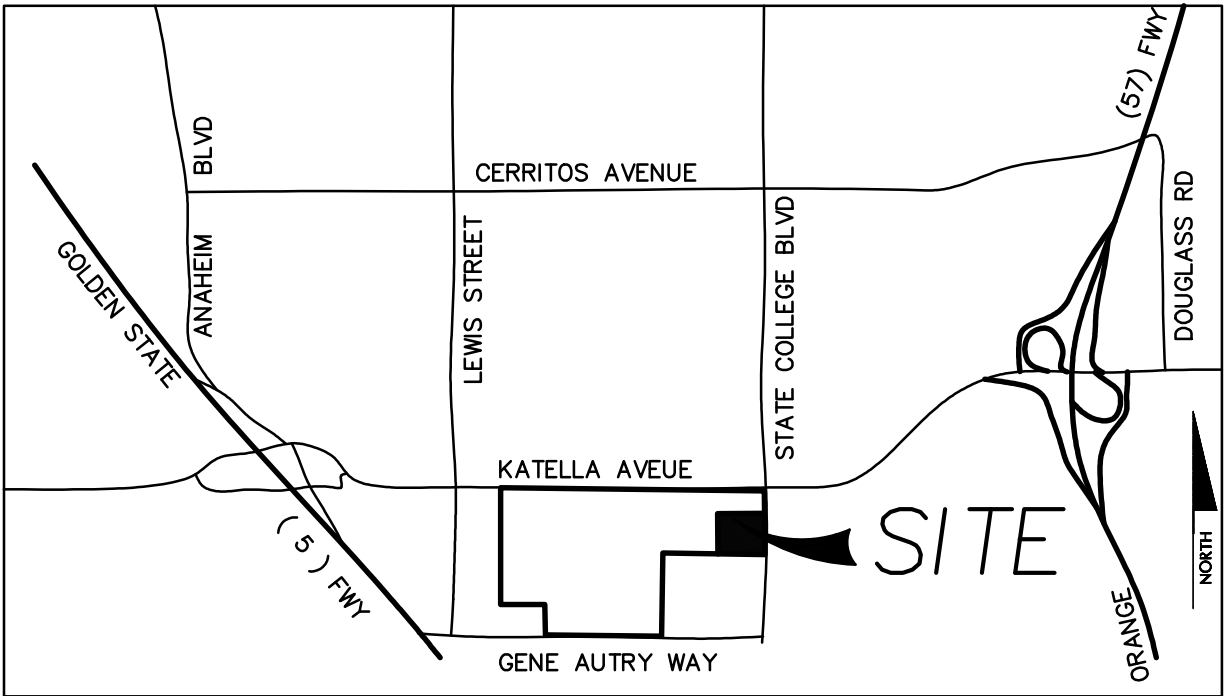
The methodology used to determine the peak discharges for A-Town is based upon the criteria set forth in the *Orange County Flood Control District Hydrology Manual* dated 1986 as incorporated in the Advanced Engineering Software (AES) “RATSC” Program. The hydrologic soil types were determined from the Hydrologic Classification of Soils map contained in the *Orange County Hydrology Manual*.

## **D. DISCUSSION**

Per the current Site Plan, storm runoff produced from Area E-1 of DA-E will drain toward the west and confluence with Area F-1 of DA-F, and then discharge into the existing 18” RCP, line “E-2”, Plan no. 36208.

The remainder area of DA-E will drain toward the north and discharge into the existing 24” RCP, line “D”, Plan no. 26195.

First flush flows produced from the site are collected in the proposed inlets throughout the site, then being diverted in the proposed diversion structures to drain to proposed Modular Wetland Systems. Treated flows are then stored in the proposed Storage Vaults. Water quality structures are shown on the hydrology map with dimensions and are addressed in details in a separate WQMP report.



# ***VICINITY MAP***



**LEGEND**

A	B	C	D	HYDROLOGIC SOIL GROUPS
				HYDROLOGIC SOIL GROUP BOUNDARY
				COUNTY BOUNDARY

## **SECTION 2**



# **HYDROLOGY CALCULATIONS**

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2016 Advanced Engineering Software (aes)  
Ver. 23.0 Release Date: 07/01/2016 License ID 1239

Analysis prepared by:

HUNSAKER & ASSOCIATES  
Irvine, Inc  
Planning \* Engineering \* Surveying  
Three Hughes \* Irvine, California 92618 \* (949)583-1010

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* W.O. # 3916-65, TRACT 17703, LOT 4, AREA 'E' \*  
\* 2-YR STUDY \*  
\* PROPOSED CONDITION \*  
\*\*\*\*\*

FILE NAME: 17703E.DAT  
TIME/DATE OF STUDY: 19:37 06/02/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	MANING: HIKE (FT)	FACTOR: (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
-----

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
ELEVATION DATA: UPSTREAM(FEET) = 152.00 DOWNSTREAM(FEET) = 151.40

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.995  
\* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.440  
SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.21	0.40	0.200	17	10.99

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 1.48  
TOTAL AREA(ACRES) = 1.21 PEAK FLOW RATE(CFS) = 1.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 12.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 151.40 DOWNSTREAM(FEET) = 150.30  
FLOW LENGTH(FEET) = 505.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.34  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.48  
PIPE TRAVEL TIME(MIN.) = 3.60 Tc(MIN.) = 14.59  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.59  
RAINFALL INTENSITY(INCH/HR) = 1.22  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 1.21  
TOTAL STREAM AREA(ACRES) = 1.21  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.48

\*\*\*\*\*  
FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.30 DOWNSTREAM(FEET) = 152.20

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.211  
\* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.703  
SUBAREA Tc AND LOSS RATE DATA(AMC I):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
RESIDENTIAL  
"11+ DWELLINGS/ACRE" A 1.50 0.40 0.200 17 8.21  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 2.19  
TOTAL AREA(ACRES) = 1.50 PEAK FLOW RATE(CFS) = 2.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.21  
RAINFALL INTENSITY(INCH/HR) = 1.70  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 1.50  
TOTAL STREAM AREA(ACRES) = 1.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.19

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	1.48	14.59	1.224	0.40( 0.08)	0.20	1.2	1.00
2	2.19	8.21	1.703	0.40( 0.08)	0.20	1.5	11.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.37	8.21	1.703	0.40( 0.08)	0.20	2.2	11.00
2	3.03	14.59	1.224	0.40( 0.08)	0.20	2.7	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.37 Tc(MIN.) = 8.21  
EFFECTIVE AREA(ACRES) = 2.18 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 2.7  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.00 TO NODE 3.10 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 220.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 152.50

Tc = K \* [(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.599  
\* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.780  
SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	0.73	0.40	0.200	17	7.60

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 1.12  
TOTAL AREA(ACRES) = 0.73 PEAK FLOW RATE(CFS) = 1.12

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.10 TO NODE 4.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 152.50 DOWNSTREAM(FEET) = 151.90  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.10  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.12  
PIPE TRAVEL TIME(MIN.) = 2.38 Tc(MIN.) = 9.98  
LONGEST FLOWPATH FROM NODE 3.00 TO NODE 4.00 = 520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 9.98  
\* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.522  
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.25	0.40	0.200	17

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
 SUBAREA AREA(ACRES) = 1.25 SUBAREA RUNOFF(CFS) = 1.62  
 EFFECTIVE AREA(ACRES) = 1.98 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.08  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.40 AREA-AVERAGED  $A_p$  = 0.20  
 TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 2.57

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 31  
 =====

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 151.90 DOWNSTREAM(FEET) = 151.60  
 FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.89  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.57  
 PIPE TRAVEL TIME(MIN.) = 0.66  $T_c$ (MIN.) = 10.64  
 LONGEST FLOWPATH FROM NODE 3.00 TO NODE 5.00 = 635.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81  
 =====

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE  $T_c$ (MIN.) = 10.64  
 \* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.467  
 SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	A	1.30	0.40	0.100	17

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
 SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 1.67  
 EFFECTIVE AREA(ACRES) = 3.28 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.06  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.40 AREA-AVERAGED  $A_p$  = 0.16  
 TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 4.14

=====

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 3.3  $T_c$ (MIN.) = 10.64  
 EFFECTIVE AREA(ACRES) = 3.28 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.06  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.40 AREA-AVERAGED  $A_p$  = 0.160  
 PEAK FLOW RATE(CFS) = 4.14

=====

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2016 Advanced Engineering Software (aes)  
Ver. 23.0 Release Date: 07/01/2016 License ID 1239

Analysis prepared by:

HUNSAKER & ASSOCIATES  
Irvine, Inc  
Planning \* Engineering \* Surveying  
Three Hughes \* Irvine, California 92618 \* (949)583-1010

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* W.O. # 3916-65, TRACT 17703, LOT 4, AREA 'E' \*  
\* 10-YR STUDY \*  
\* PROPOSED CONDITION \*  
\*\*\*\*\*

FILE NAME: 17703E.DAT  
TIME/DATE OF STUDY: 19:39 06/02/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	MANINGG HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21  
\*\*\*\*\*

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
ELEVATION DATA: UPSTREAM(FEET) = 152.00 DOWNSTREAM(FEET) = 151.40

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.995  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.585  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.21	0.40	0.200	32	10.99

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 2.73  
TOTAL AREA(ACRES) = 1.21 PEAK FLOW RATE(CFS) = 2.73

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 12.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 151.40 DOWNSTREAM(FEET) = 150.30  
FLOW LENGTH(FEET) = 505.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.74  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.73  
PIPE TRAVEL TIME(MIN.) = 3.08 Tc(MIN.) = 14.07  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.07  
RAINFALL INTENSITY(INCH/HR) = 2.24  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 1.21  
TOTAL STREAM AREA(ACRES) = 1.21  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.30 DOWNSTREAM(FEET) = 152.20

Tc = K \* [(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.211  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.055  
SUBAREA Tc AND LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
RESIDENTIAL  
"11+ DWELLINGS/ACRE" A 1.50 0.40 0.200 32 8.21  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 4.02  
TOTAL AREA(ACRES) = 1.50 PEAK FLOW RATE(CFS) = 4.02

\*\*\*\*\*  
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.21  
RAINFALL INTENSITY(INCH/HR) = 3.06  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 1.50  
TOTAL STREAM AREA(ACRES) = 1.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.02

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.73	14.07	2.244	0.40( 0.08)	0.20	1.2	1.00
2	4.02	8.21	3.055	0.40( 0.08)	0.20	1.5	11.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.20	8.21	3.055	0.40( 0.08)	0.20	2.2	11.00
2	5.65	14.07	2.244	0.40( 0.08)	0.20	2.7	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.20 Tc(MIN.) = 8.21  
EFFECTIVE AREA(ACRES) = 2.21 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 2.7  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.00 TO NODE 3.10 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 220.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 152.50

Tc = K \* [(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.599  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.194  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	0.73	0.40	0.200	32	7.60

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 2.05  
TOTAL AREA(ACRES) = 0.73 PEAK FLOW RATE(CFS) = 2.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.10 TO NODE 4.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 152.50 DOWNSTREAM(FEET) = 151.90  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.47  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.05  
PIPE TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 9.62  
LONGEST FLOWPATH FROM NODE 3.00 TO NODE 4.00 = 520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 9.62  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.790  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.25	0.40	0.200	32



SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
 SUBAREA AREA (ACRES) = 1.25 SUBAREA RUNOFF (CFS) = 3.05  
 EFFECTIVE AREA (ACRES) = 1.98 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.08  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.40 AREA-AVERAGED  $A_p$  = 0.20  
 TOTAL AREA (ACRES) = 2.0 PEAK FLOW RATE (CFS) = 4.83

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 151.90 DOWNSTREAM (FEET) = 151.60  
 FLOW LENGTH (FEET) = 115.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.0 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.28  
 ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 4.83  
 PIPE TRAVEL TIME (MIN.) = 0.58  $T_c$  (MIN.) = 10.21  
 LONGEST FLOWPATH FROM NODE 3.00 TO NODE 5.00 = 635.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE  $T_c$  (MIN.) = 10.21  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.697  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	A	1.30	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
 SUBAREA AREA (ACRES) = 1.30 SUBAREA RUNOFF (CFS) = 3.11  
 EFFECTIVE AREA (ACRES) = 3.28 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.06  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.40 AREA-AVERAGED  $A_p$  = 0.16  
 TOTAL AREA (ACRES) = 3.3 PEAK FLOW RATE (CFS) = 7.77

=====

END OF STUDY SUMMARY:  
 TOTAL AREA (ACRES) = 3.3  $T_c$  (MIN.) = 10.21  
 EFFECTIVE AREA (ACRES) = 3.28 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.06  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.40 AREA-AVERAGED  $A_p$  = 0.160  
 PEAK FLOW RATE (CFS) = 7.77

=====

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* W.O. # 3916-65, TRACT 17703, LOT 4, AREA 'E' \*  
\* 25-YR STUDY \*  
\* PROPOSED CONDITION \*  
\*\*\*\*\*

FILE NAME: 17703E.DAT  
TIME/DATE OF STUDY: 19:41 06/02/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21  
\*\*\*\*\*

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
ELEVATION DATA: UPSTREAM (FEET) = 152.00 DOWNSTREAM (FEET) = 151.40

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$  (MIN.) = 10.995  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.088  
SUBAREA  $T_c$  AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE / LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.21	0.40	0.200	32	10.99

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
SUBAREA RUNOFF (CFS) = 3.28  
TOTAL AREA (ACRES) = 1.21 PEAK FLOW RATE (CFS) = 3.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 12.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 151.40 DOWNSTREAM(FEET) = 150.30
FLOW LENGTH(FEET) = 505.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.85
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.28
PIPE TRAVEL TIME(MIN.) = 2.95 Tc(MIN.) = 13.95
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.95
RAINFALL INTENSITY(INCH/HR) = 2.70
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 1.21
TOTAL STREAM AREA(ACRES) = 1.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.28

\*\*\*\*\*
FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00
ELEVATION DATA: UPSTREAM(FEET) = 154.30 DOWNSTREAM(FEET) = 152.20

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.211
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.643
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" A 1.50 0.40 0.200 32 8.21
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 4.81
TOTAL AREA(ACRES) = 1.50 PEAK FLOW RATE(CFS) = 4.81

\*\*\*\*\*
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.21
RAINFALL INTENSITY(INCH/HR) = 3.64
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 1.50
TOTAL STREAM AREA(ACRES) = 1.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.81

\*\* CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	3.28	13.95	2.699	0.40( 0.08)	0.20	1.2
2	4.81	8.21	3.643	0.40( 0.08)	0.20	1.5

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	7.43	8.21	3.643	0.40( 0.08)	0.20	2.2	11.00
2	6.81	13.95	2.699	0.40( 0.08)	0.20	2.7	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.43 Tc(MIN.) = 8.21  
EFFECTIVE AREA(ACRES) = 2.21 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 2.7  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.00 TO NODE 3.10 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 220.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 152.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.599  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.806  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	0.73	0.40	0.200	32	7.60

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 2.45  
TOTAL AREA(ACRES) = 0.73 PEAK FLOW RATE(CFS) = 2.45

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.10 TO NODE 4.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 152.50 DOWNSTREAM(FEET) = 151.90  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.58  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.45  
PIPE TRAVEL TIME(MIN.) = 1.93 Tc(MIN.) = 9.53  
LONGEST FLOWPATH FROM NODE 3.00 TO NODE 4.00 = 520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 9.53  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.348  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.25	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA AREA (ACRES) = 1.25 SUBAREA RUNOFF (CFS) = 3.68  
 EFFECTIVE AREA (ACRES) = 1.98 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.08  
 AREA-AVERAGED  $F_p$  (INCH/HR) = 0.40 AREA-AVERAGED  $A_p = 0.20$   
 TOTAL AREA (ACRES) = 2.0 PEAK FLOW RATE (CFS) = 5.82

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 151.90 DOWNSTREAM (FEET) = 151.60  
 FLOW LENGTH (FEET) = 115.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.7 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.51  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 5.82  
 PIPE TRAVEL TIME (MIN.) = 0.55  $T_c$  (MIN.) = 10.08  
 LONGEST FLOWPATH FROM NODE 3.00 TO NODE 5.00 = 635.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE  $T_c$  (MIN.) = 10.08  
 \* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.244  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	A	1.30	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA AREA (ACRES) = 1.30 SUBAREA RUNOFF (CFS) = 3.75  
 EFFECTIVE AREA (ACRES) = 3.28 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.06  
 AREA-AVERAGED  $F_p$  (INCH/HR) = 0.40 AREA-AVERAGED  $A_p = 0.16$   
 TOTAL AREA (ACRES) = 3.3 PEAK FLOW RATE (CFS) = 9.39

=====

END OF STUDY SUMMARY:  
 TOTAL AREA (ACRES) = 3.3  $T_c$  (MIN.) = 10.08  
 EFFECTIVE AREA (ACRES) = 3.28 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.06  
 AREA-AVERAGED  $F_p$  (INCH/HR) = 0.40 AREA-AVERAGED  $A_p = 0.160$   
 PEAK FLOW RATE (CFS) = 9.39

-----  
 END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* W.O. # 3916-65, TRACT 17703, LOT 4, AREA 'E' \*  
\* 100-YR STUDY \*  
\* PROPOSED CONDITION \*  
\*\*\*\*\*

FILE NAME: 17703E.DAT  
TIME/DATE OF STUDY: 19:42 06/02/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21  
\*\*\*\*\*

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
ELEVATION DATA: UPSTREAM (FEET) = 152.00 DOWNSTREAM (FEET) = 151.40

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 10.995  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.939  
SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.21	0.40	0.200	52	10.99

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF (CFS) = 4.20  
TOTAL AREA (ACRES) = 1.21 PEAK FLOW RATE (CFS) = 4.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 12.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 151.40 DOWNSTREAM(FEET) = 150.30
FLOW LENGTH(FEET) = 505.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.98
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.20
PIPE TRAVEL TIME(MIN.) = 2.82 Tc(MIN.) = 13.82
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.82
RAINFALL INTENSITY(INCH/HR) = 3.46
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 1.21
TOTAL STREAM AREA(ACRES) = 1.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.20

\*\*\*\*\*
FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00
ELEVATION DATA: UPSTREAM(FEET) = 154.30 DOWNSTREAM(FEET) = 152.20

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.211
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.657
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" A 1.50 0.40 0.200 52 8.21
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 6.18
TOTAL AREA(ACRES) = 1.50 PEAK FLOW RATE(CFS) = 6.18

\*\*\*\*\*
FLOW PROCESS FROM NODE 12.00 TO NODE 12.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.21
RAINFALL INTENSITY(INCH/HR) = 4.66
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 1.50
TOTAL STREAM AREA(ACRES) = 1.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.18

\*\* CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	4.20	13.82	3.456	0.40( 0.08)	0.20	1.2 1.00
2	6.18	8.21	4.657	0.40( 0.08)	0.20	1.5 11.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	9.56	8.21	4.657	0.40( 0.08)	0.20	2.2	11.00
2	8.76	13.82	3.456	0.40( 0.08)	0.20	2.7	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.56 Tc(MIN.) = 8.21  
EFFECTIVE AREA(ACRES) = 2.22 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 2.7  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 805.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.00 TO NODE 3.10 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 220.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 152.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.599  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.868  
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	0.73	0.40	0.200	52	7.60

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 3.15  
TOTAL AREA(ACRES) = 0.73 PEAK FLOW RATE(CFS) = 3.15

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.10 TO NODE 4.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 152.50 DOWNSTREAM(FEET) = 151.90  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.73  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.15  
PIPE TRAVEL TIME(MIN.) = 1.83 Tc(MIN.) = 9.43  
LONGEST FLOWPATH FROM NODE 3.00 TO NODE 4.00 = 520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 9.43  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.302  
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	A	1.25	0.40	0.200	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200



SUBAREA AREA (ACRES) = 1.25      SUBAREA RUNOFF (CFS) = 4.75  
 EFFECTIVE AREA (ACRES) = 1.98      AREA-AVERAGED Fm (INCH/HR) = 0.08  
 AREA-AVERAGED Fp (INCH/HR) = 0.40      AREA-AVERAGED Ap = 0.20  
 TOTAL AREA (ACRES) = 2.0      PEAK FLOW RATE (CFS) = 7.52

\*\*\*\*\*  
 FLOW PROCESS FROM NODE      4.00 TO NODE      5.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 151.90      DOWNSTREAM (FEET) = 151.60  
 FLOW LENGTH (FEET) = 115.00      MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.8 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.64  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00      NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 7.52  
 PIPE TRAVEL TIME (MIN.) = 0.53      Tc (MIN.) = 9.96  
 LONGEST FLOWPATH FROM NODE      3.00 TO NODE      5.00 = 635.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE      5.00 TO NODE      5.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 9.96  
 \* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.170  
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	1.30	0.40	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 1.30      SUBAREA RUNOFF (CFS) = 4.83  
 EFFECTIVE AREA (ACRES) = 3.28      AREA-AVERAGED Fm (INCH/HR) = 0.06  
 AREA-AVERAGED Fp (INCH/HR) = 0.40      AREA-AVERAGED Ap = 0.16  
 TOTAL AREA (ACRES) = 3.3      PEAK FLOW RATE (CFS) = 12.12

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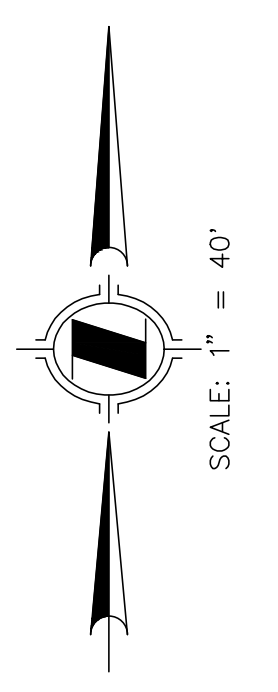
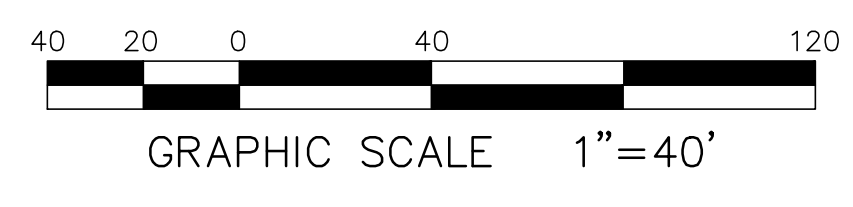
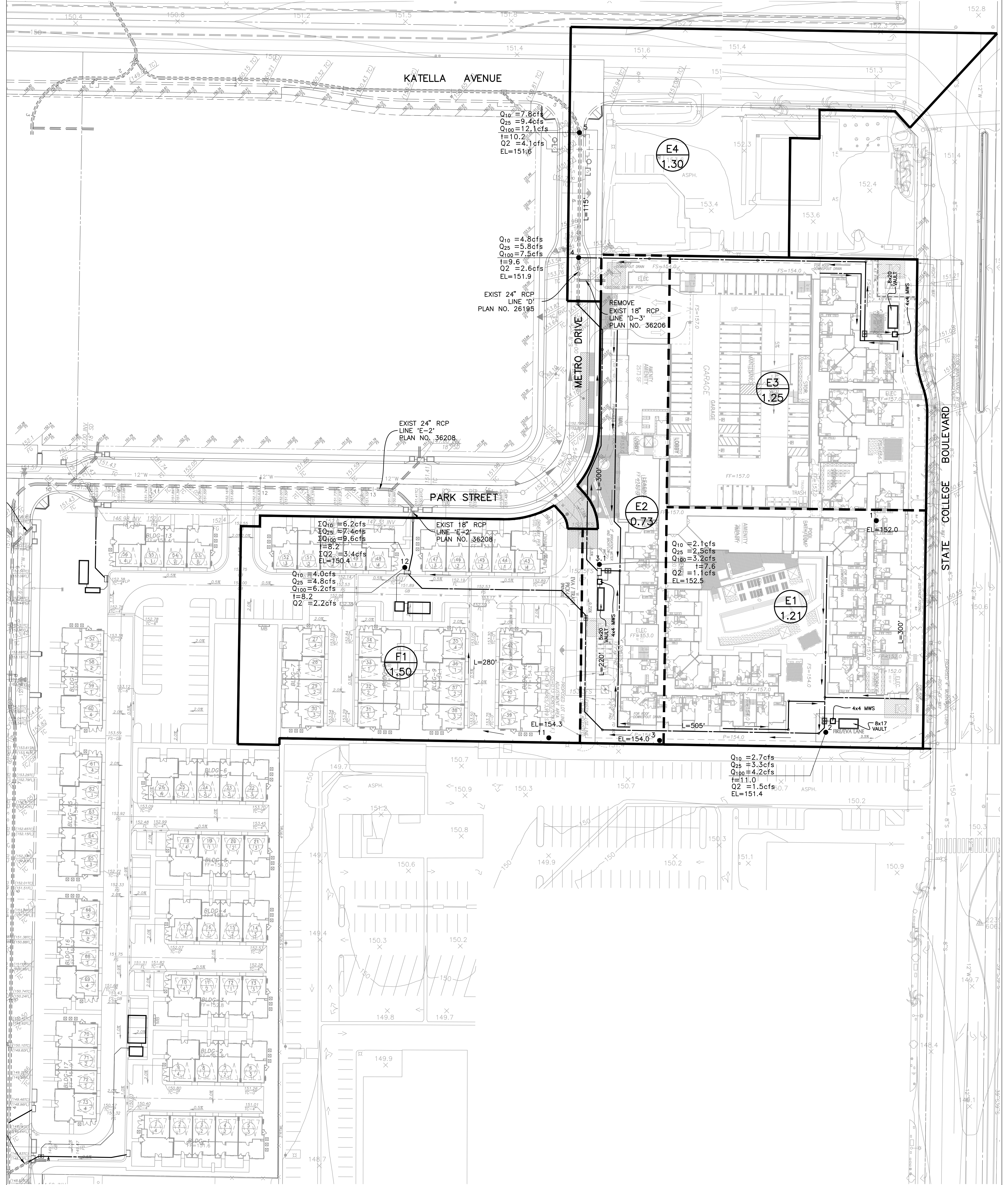
END OF STUDY SUMMARY:  
 TOTAL AREA (ACRES) = 3.3      TC (MIN.) = 9.96  
 EFFECTIVE AREA (ACRES) = 3.28      AREA-AVERAGED Fm (INCH/HR) = 0.06  
 AREA-AVERAGED Fp (INCH/HR) = 0.40      AREA-AVERAGED Ap = 0.160  
 PEAK FLOW RATE (CFS) = 12.12

=====

END OF RATIONAL METHOD ANALYSIS

## **SECTION 3**

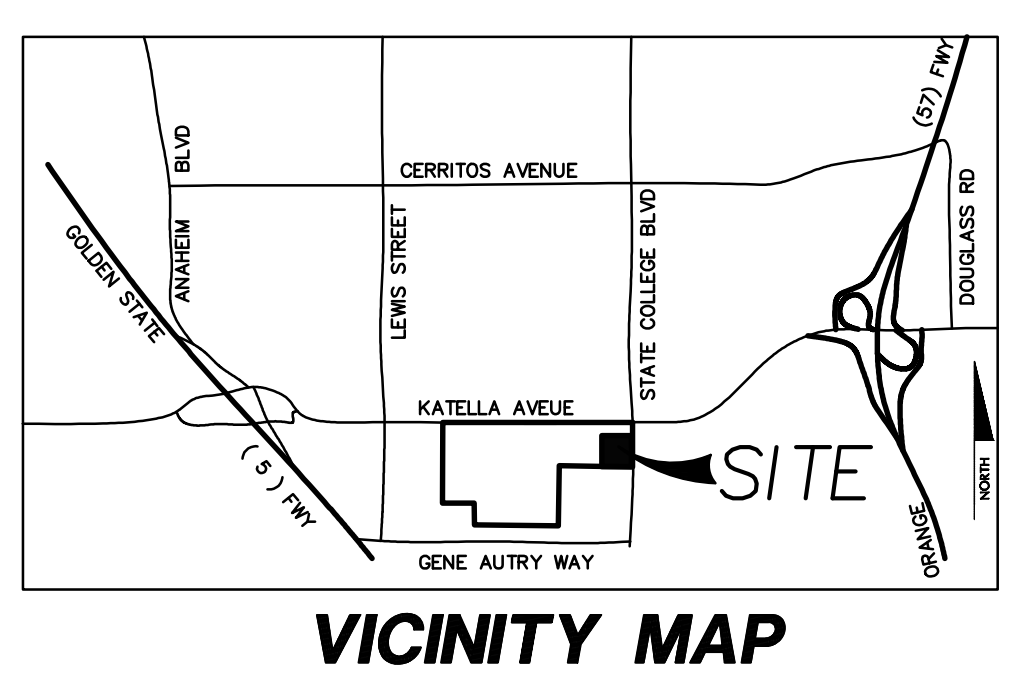
# HYDROLOGY MAP



PREPARED BY:  
**HUNSAKER & ASSOCIATES**  
 IRVINE, INC.  
 PLANNING ■ ENGINEERING ■ SURVEYING  
 Three Hughes ■ Irvine, CA 92618 ■ PH: (949) 583-1010 ■ FX: (949) 583-0759

**PRELIMINARY HYDROLOGY MAP**  
**FOR**  
**A-TOWN TRACT NO. 17703**  
**LOT 4 - AREA E**

- LEGEND**
- MAJOR DRAINAGE BOUNDARY
  - - - MINOR DRAINAGE BOUNDARY
  - 1. NODE NUMBER
  - (A) AREA DESIGNATION
  - (1.0) AREA ACREAGE (IN ACRES)
  - $Q_{10} = 6.0\text{cfs}$   
 $Q_{25} = 8.0\text{cfs}$   
 $Q_{100} = 10.0\text{cfs}$   
 $t = 10$   
 $Q_2 = 1$  PEAK FLOW RATE  
TIME OF CONCENTRATION
  - $EQ_{10} = 8.0\text{cfs}$   
 $EQ_{25} = 10.0\text{cfs}$   
 $t = 15.0$  PEAK CONFLUENCE FLOW RATE  
TIME OF CONCENTRATION
  - PROPOSED STORM DRAIN
  - SOIL GROUP



## **SECTION 4**

# REFERENCES

**APPROVED**  
**SD IMPROVEMENT PLANS**  
**FOR A-TOWN TRACT 17703**

GENERAL NOTES

1. ALL WORK WITHIN THE RIGHT-OF WAY WILL REQUIRE A RIGHT-OF-WAY EXCAVATION & CONSTRUCTION PERMIT.
2. CONTACT THE FIELD ENGINEER AT (714) 765-5126 48 HOURS PRIOR TO ANY OF THIS WORK.
3. ALL WORK SHALL BE IN ACCORDANCE WITH THE APPLICABLE SECTIONS OF STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION, CITY OF ANAHEIM STANDARD PLANS, CONTRACT DOCUMENTS AND STANDARD SPECIFICATION SUPPLEMENT AND THE LATEST REVISIONS THEREOF."
4. THE CONTRACTOR SHALL NOTIFY UNDERGROUND SERVICE ALERT AT 1-800-422-4133 A MINIMUM OF 48 HOURS PRIOR TO START OF CONSTRUCTION WITHIN THE RIGHT-OF-WAY.
5. ALL PAVING REMOVAL SHALL BE SAWCUT AT THE FIELD ENGINEER'S DIRECTION. MINIMUM DEPTH OF CUT: 0.12'.
6. PAVING SHALL BE SAWCUT AND REMOVED A MINIMUM OF 1' FROM CURB AND GUTTER CONSTRUCTION OR RECONSTRUCTION.
7. THE PROTECTION AND ADJUSTMENT OF ALL UTILITIES SHALL BE THE RESPONSIBILITY OF THE DEVELOPER.
8. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO PROTECT AND/OR RELOCATE ALL TRAFFIC SIGNS AND TRAFFIC SIGNALS AS SHOWN ON THE PLANS OR AS REQUIRED BY THE FIELD ENGINEER.
9. IRRIGATION LINES SHALL BE REMOVED, RELOCATED OUT OF THE STREET RIGHT-OF-WAY, ENCASED IN A STEEL SLEEVE, OR REPLACED WITH CAST IRON AS DIRECTED BY THE PARKS DIVISION. NOTIFY THE PARKS DIVISION AT (714) 765-5155 48 HOURS PRIOR TO WORK.
10. REPORTS OF COMPACTION WITHIN THE RIGHT-OF-WAY SHALL BE SUBMITTED TO AND ACCEPTED BY THE FIELD ENGINEER PRIOR TO PLACING ANY PAVING.
11. IN THE EVENT THAT EXISTING STRIPING IS OBLITERATED BY CONSTRUCTION, IT WILL BE THE RESPONSIBILITY OF THE DEVELOPER TO REPLACE SAID STRIPING.
12. PRIOR TO CONSTRUCTION, ALL SURVEY POINTS THAT MAY BE DISTURBED SHALL BE TIED OUT AND A CORNER RECORD OF EACH POINT SHALL BE FILED WITH THE COUNTY SUPERVISOR. A COPY OF THE RECORDED CORNER RECORD SHALL BE SUBMITTED TO THE CITY'S FIELD SERVICES DIVISION. FOLLOWING THE COMPLETION OF THE CONSTRUCTION, A CORNER RECORD OF EACH POINT THAT WAS DISTURBED SHALL BE FILED WITH THE COUNTY SURVEYOR. A COPY OF THE RECORDED CORNER RECORD SHALL BE SUBMITTED TO THE CITY'S FIELD SERVICES DIVISION PRIOR TO THE RECORDING OF A CERTIFICATE OF COMPLETION OR RELEASE OF BONDS.

GENERAL NOTES FOR STORM DRAIN AND SEWER IMPROVEMENT PLANS

1. PRIOR TO DELIVERY OF STORM DRAIN PIPES, CONTACT FIELD ENGINEERING AT (714) 765-5126 FOR D-LOAD TEST APPROVAL.
2. THE CONTRACTOR SHALL CHECK THE FLOW LINE ELEVATION OF EXISTING JUNCTURE AGAINST CONTROL PROVIDED PRIOR TO CONSTRUCTION. IF THE EXISTING FLOW LINE VARIES FROM THE PLAN ELEVATION BY MORE THAN ±0.10' THE ENGINEER SHALL ADJUST THE GRADES BETWEEN THE JUNCTURE AND THE NEXT UPSTREAM MANHOLE, WITH THE APPROVAL OF THE FIELD ENGINEER.
3. ADJUST ALL MANHOLES TO GRADE AFTER PLACING FINAL LIFT OF ASPHALT.
4. 2-SACK SAND CEMENT SLURRY TRENCH BACKFILL SHALL BE REQUIRED TO 1' ABOVE THE FINISH TOP OF PIPE WHERE LINE IS CONSTRUCTED AT A SLOPE OF 5:1 OR MORE.
5. CERTIFICATION BY A LICENSED SURVEYOR OR REGISTERED CIVIL ENGINEER SHALL BE SUBMITTED PRIOR TO FINAL ACCEPTANCE CERTIFYING THAT THE STORM DRAIN SYSTEM WAS INSTALLED ON GRADE PER APPROVED PLAN.

BASIS OF BEARINGS:

BEARINGS SHOWN HEREON ARE BASED UPON THE BEARINGS BETWEEN O.C.S. HORIZONTAL CONTROL STATION GPS NO. 3094 AND STATION GPS NO. 3086 BEING NORTH 89°07'46" WEST PER RECORDS ON FILE IN THE OFFICE OF THE ORANGE COUNTY SURVEYOR.

LEGAL DESCRIPTION:

IN THE CITY OF ANAHEIM, COUNTY OF ORANGE, STATE OF CALIFORNIA, BEING A SUBDIVISION OF LOTS 2 THROUGH 10, INCLUSIVE, LOTS 12 THROUGH 14, INCLUSIVE, LOTS A, B, MARKET STREET, BRYANT STREET, GRANVILLE DRIVE, TRIAD STREET, UNION STREET, MERIDIAN LANE, METRO DRIVE, PARK LANE, KATELLA AVENUE, GENE AUTRY WAY, STATE COLLEGE BOULEVARD AND WESTSIDE DRIVE OF TRACT NO. 16859 AS SHOWN ON A MAP RECORDED IN BOOK 892, PAGES 1 THROUGH 10, INCLUSIVE, OF MISCELLANEOUS MAPS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY.

NOTICE TO CONTRACTOR PRIOR TO CONSTRUCTION

BEFORE PROCEEDING WITH THIS WORK, THE CONTRACTOR SHALL CAREFULLY CHECK AND VERIFY ALL CONDITIONS, QUANTITIES, DIMENSIONS AND SURFACE GRADE ELEVATIONS, UTILITY CONNECTION ELEVATIONS AND LOCATIONS AND SHALL REPORT ALL DISCREPANCIES TO THE ENGINEER PRIOR TO THE COMMENCEMENT OF WORK.

UNAUTHORIZED CHANGES & USES: THE ENGINEER PREPARING THESE PLANS WILL NOT BE RESPONSIBLE FOR, OR LIABLE FOR, UNAUTHORIZED CHANGES TO, DELETIONS FROM OR USES OF THESE PLANS. ALL CHANGES TO THE PLANS MUST BE PRESENTED IN WRITING AND MUST BE APPROVED BY THE PREPARER OF THESE PLANS AND THE ENGINEER OF RECORD IN WRITING.

CONTRACTOR SHALL IMPLEMENT AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH EROSION CONTROL PLAN GRA.

UNDERGROUND SERVICE ALERT

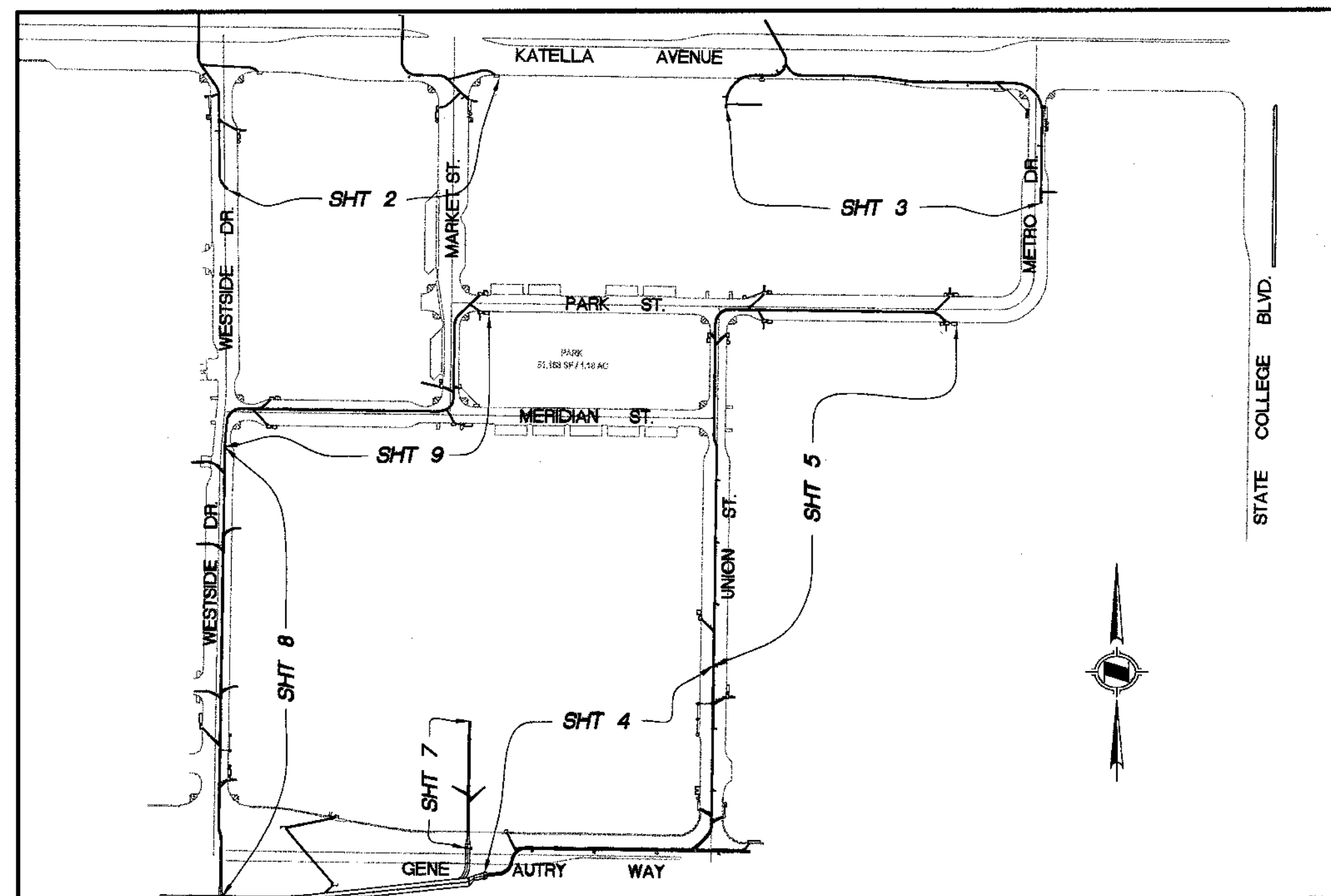
Call: Toll FREE  
1-800-422-4133  
TWO WORKING DAYS BEFORE YOU DIG

"CAUTION": Remember that the USA Center notifies only those utilities belonging to the center. There could be other utilities present at the work site. The center will inform you of whom they will notify.

THESE PLANS HAVE BEEN EXAMINED AND IS APPROVED ONLY AS TO COMPATIBILITY WITH ADJOINING EXISTING OR FUTURE IMPROVEMENTS AND CONFORMANCE WITH CITY OF ANAHEIM STANDARD DETAILS AND THE REQUIREMENTS FOR THE FOLLOWING APPLICABLE FACTORS: RIGHT-OF-WAY, ROADWAY MATERIALS, ALIGNMENTS AND GRADES, HYDROLOGY AND HYDRAULIC DESIGN OF STORMDRAIN OR SANITARY SEWER SYSTEMS AND UNDER GROUND CONDUIT OR OPEN CHANNEL CHANNEL ALIGNMENTS, GRADES, SIZES AND MATERIALS.

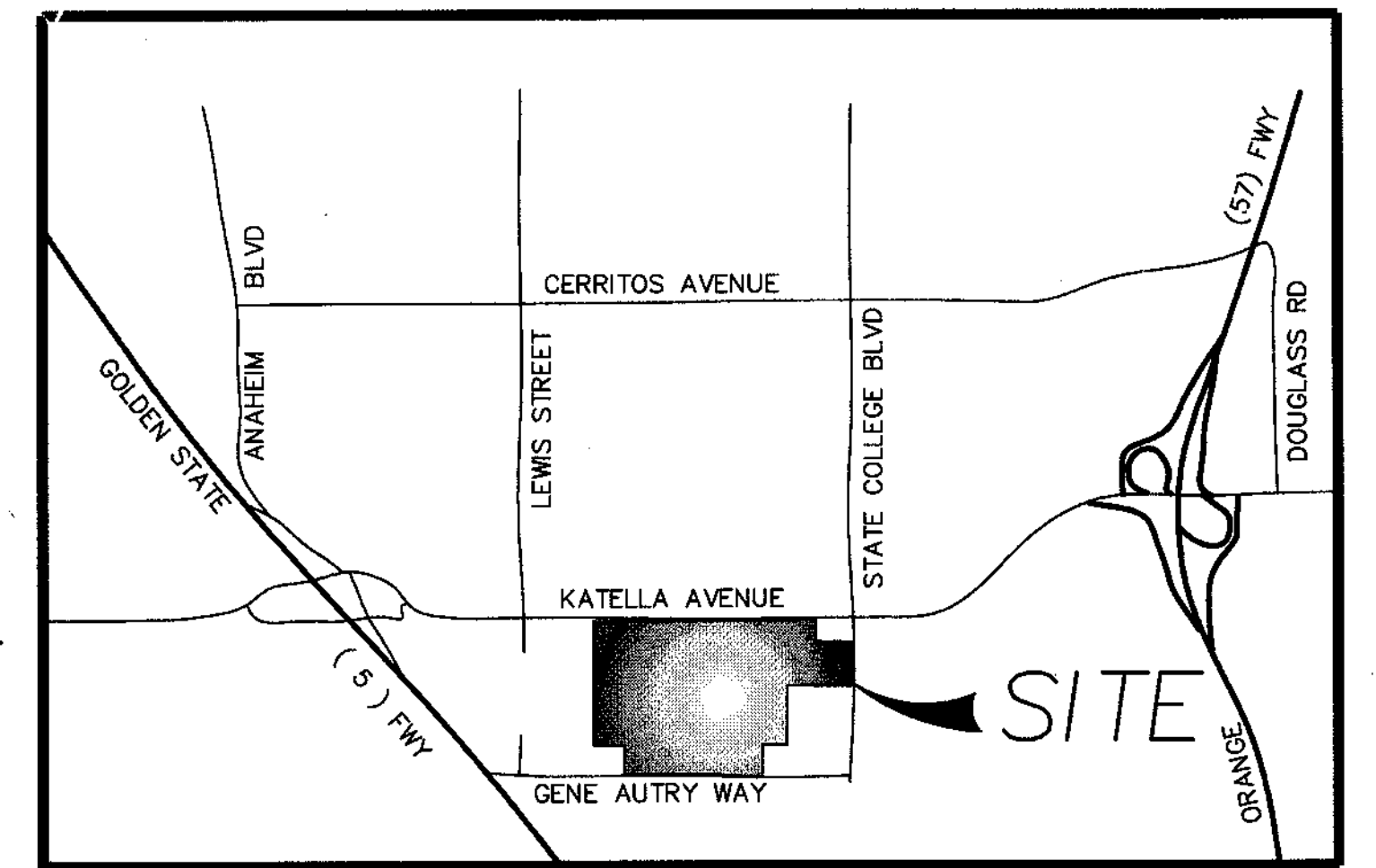
ENGINEER'S NOTE TO CONTRACTOR : THE EXISTENCE LOCATION OF ANY UNDERGROUND UTILITIES, PIPES, AND/OR STRUCTURES SHOWN ON THESE PLANS WERE OBTAINED BY A SEARCH OF AVAILABLE RECORDS, TO THE BEST OF OUR KNOWLEDGE, THERE ARE NO EXISTING UTILITIES EXCEPT AS SHOWN ON THESE PLANS. THE CONTRACTOR SHALL AS CERTAIN THE TRUE VERTICAL AND HORIZONTAL LOCATION AND SIZE OF THOSE TO BE USED OF ANY UNDERGROUND UTILITIES AND SHALL BE RESPONSIBLE FOR DAMAGE TO ANY PUBLIC OR PRIVATE UTILITIES AS SHOWN HEREON.

# CITY OF ANAHEIM STORM DRAIN IMPROVEMENT PLANS FOR TRACT 17703



INDEX MAP

SCALE: 1" = 200'



VICINITY MAP

CONSTRUCTION NOTES & QUANTITY ESTIMATE

NO.	DESCRIPTION	AMOUNT	UNIT
47	CONST MODIFIED J.S. PER SPPWC STD PLAN NO 333-2, DETAIL ON SHEET 8	1	EA.
48	INST. 1'H x 6'W R.C.B.	8	L.F.
49	REMOVE PLUG AND JOIN EXISTING	4	EA.
50	TRANS. FROM 1'H x 6'W RCB TO 30" RCP PER SPPWC STD. PLAN NO. 342-2	17.5	L.F.
51	CONST. CONCRETE COLLAR PER SPPWC STD. PLAN NO. 380-4	6	EA.
52	CONST. J.S. PER SPPWC STD. PLAN NO. 331-3	15	EA.
53	INST. 18" RCP (SEE PROFILE FOR D-LOAD) BEDDING PER OCPW STD. NO. 1319, DETAIL ON SHEET 13	552	L.F.
54	INST. 30" RCP (SEE PROFILE FOR D-LOAD) BEDDING PER OCPW STD. NO. 1319, DETAIL ON SHEET 13	551	L.F.
56	CONST THE MAXWELL IV AUXILIARY PER TORRENT RESOURCES, DETAIL ON SHT. 12	3	EA.
57	INST. 22.5" ELBOW	3	EA.
58	CONST. C.B. PER CITY OF ANAHEIM STD. DETAIL NO. 300-2, CASE A WITH AUTOMATIC RETRACTABLE SCREEN & CONNECTOR PIPE SCREEN **	18	EA.
59	CONST. DOUBLE BRICK AND MORTAR PLUG	5	EA.
60	INST. 24" RCP (SEE PROFILE FOR D-LOAD) BEDDING PER OCPW STD. NO. 1319, DETAIL ON SHEET 13	1323	L.F.
61	CONST. M.H. PER SPPWC STD. PLAN NO. 321-2	6	EA.
62	CONST. BLANKET PROTECTION PER SPPWC STD. PLAN NO. 225-2 WITH 2 SACK CEMENT SAND SLURRY (NO CONCRETE)	36	L.F.
63	INST. 4" SCH-80 PVC OUTLET PIPE	150	L.F.
64	CONST. THE MAXWELL IV PER TORRENT RESOURCES, DETAIL ON SHEET 13	9	EA.
65	CONST. 4'x10' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE	2	EA.
66	CONST. 4'x12' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE	2	EA.
67	CONST. 4'x16' FILTERRA BOX WITH 6" SCH-80 PVC OUTLET PIPE	1	EA.
68	CONST. MODIFIED MH PER SPPWC STD PLAN NO 321-2, DETAIL ON SHEET 12	1	EA.
69	CONST. MODIFIED MH PER SPPWC STD PLAN NO 321-2, DETAIL ON SHEET 12	1	EA.
70	CONST. 4'x4' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE	4	EA.
71	CONST. 4'x6' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE	7	EA.
72	CONST. 4'x8' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE	4	EA.
76	CONST. 6'x8' FILTERRA BOX WITH 6" SCH-80 PVC OUTLET PIPE	2	EA.
77	CONST. AUTOMATIC RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN ON EX. CATCH BASIN **	5	EA.
80	INST. 6" SCH-80 PVC OUTLET PIPE	-	L.F.

\*\* INSTALL AUTOMATIC RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN. RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN SHALL BE CONSTRUCTED OF CORROSION RESISTANT MATERIALS AND SHALL BE "FULL CAPTURE" DESIGN AND OF MAINTAINABLE DESIGN. CONTRACTOR SHALL MAKE PRODUCT SUBMITTAL TO ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION.

NOTE: - SUPPORT FOR CONDUITS ACROSS TRENCHES PER SPPWC STD. PLAN NO. 224-2  
- TRENCH REPLACEMENT PER CITY OF ANAHEIM STD. DETAIL NO. 132-C

ABBREVIATIONS

- FS FINISH SURFACE
- TC TOP OF CURB
- FL FLOW LINE
- CL CENTER LINE
- BC BEGIN CURVE
- EC END CURVE
- W WATER
- S SEWER
- CB CATCH BASIN
- LF LINEAR FEET
- HGL HYDRAULIC GRADE LINE
- EA EACH
- MH MANHOLE
- JS JUNCTION STRUCTURE
- RCP REINFORCED CONCRETE PIPE
- PRC POINT OF REVERSE CURVE

INDEX OF SHEETS:

- PLAN NO.
- SHEET 1 - 36204 - TITLE SHEET
- SHEET 2 - 36205 - EX. LINE 'A-1' EXTENSION, LINE 'A-3' & EX. LINE 'B-2' EXTENSION
- SHEET 3 - 36206 - AS-BUILT LINES 'C' & 'D'
- SHEET 4 - 36207 - AS-BUILT LINES 'E', 'E-1', 'E-2', 'E-3', 'E-2a' & 'E-2b'
- SHEET 5 - 36208 - LINE 'E-2' EXTENSION
- SHEET 6 - 36209 - LINES 'E-2c' - 'E-2i'
- SHEET 7 - 36210 - AS-BUILT LINE 'F' PLAN NO. 26198
- SHEET 8 - 36211 - LINES 'G' FR. STA. 10+00.00 TO 17+22.26, 'G-1' & 'G-2'
- SHEET 9 - 36212 - LINES 'G' FROM STA. 17+22.26 TO 23+33.71, 'G-8' & 'G-9'
- SHEET 10 - 36213 - LINES 'G-3' - 'G-7' & 'G-10' - 'G-13'
- SHEET 11 - 36214 - DETAILS
- SHEET 12 - 36215 - STRUCTURE DETAILS
- SHEET 13 - 36216 - STRUCTURE DETAILS

I HEREBY CERTIFY THAT THE IMPROVEMENTS HAVE BEEN COMPLETED IN CONFORMANCE WITH THIS APPROVAL PLAN.

EDWARD A. MANDICH DATE  
RCE 59089  
EXP.: 06/30/17  
HUNSAKER & ASSOCIATES  
3 HUGHES, IRVINE CA 92618  
(949) 583-1010

SERVICE AGENCIES :  
CITY OF ANAHEIM, ENGINEERING DIV. (714) 765-5126  
CITY OF ANAHEIM, ELECTRICAL DEPT. (714) 765-5126  
CITY OF ANAHEIM, FIELD ENGR. (714) 765-5126  
CITY OF ANAHEIM, WATER ENGR. DIV. (714) 765-5196  
PACIFIC TELEPHONE (714) 633-0811  
SO. CALIFORNIA GAS COMPANY (714) 634-3258

ENGINEER: **HUNSAKER & ASSOCIATES**  
IRVINE, INC.  
PLANNING ■ ENGINEERING ■ SURVEYING  
Three Hughes ■ Irvine, CA 92618  
FX: (949) 583-0759 ■ PH: (949) 583-1010  
Ed Mandich 5-6-16  
EDWARD A. MANDICH, RCE NO. 59089 DATE

RCP 2015-11013  
OWNER: **PT METRO, LLC**  
25 ENTERPRISE, 3rd FLOOR  
ALISO VIEJO, CA 92656  
(949) 349-8000  
SOILS ENGINEER: **GROUP DELTA CONSULTANTS**  
32 MAUCHLY, SUITE B  
IRVINE, CA 92618  
PH: (949) 450-2100

REVISIONS

NO.	INIT.	DATE	DESCRIPTION	DATE	APP'D
1	T.T.	01/17/16	REVISED LINES 'G-2' & 'G-3' ON SHEETS 8 & 10, PLAN NO'S 36211 & 36213	01/17/16	Ed Mandich

REFERENCES

BENCH MARK: 9A-22 ELEVATION: 151.99 (NAVD88)  
KATELLA AVENUE/STATE COLLEGE BLVD.  
BRASS CAP MKD C OF A BM, IN THE TOP OF CURB AT THE SE COR.  
ELEVATION: 151.99 (NAVD88)  
PLANS FOR THESE IMPROVEMENTS: STREET: WATER: W-3175  
SEWER: 36168-36170  
STORM DRAIN: 36204-36216  
LANDSCAPE:

APPROVAL

RECOMMEND APPROVAL  
DEVELOPMENT SERVICES MANAGER  
DATE 5/25/16  
CITY ENGINEER  
DATE 5/26/16

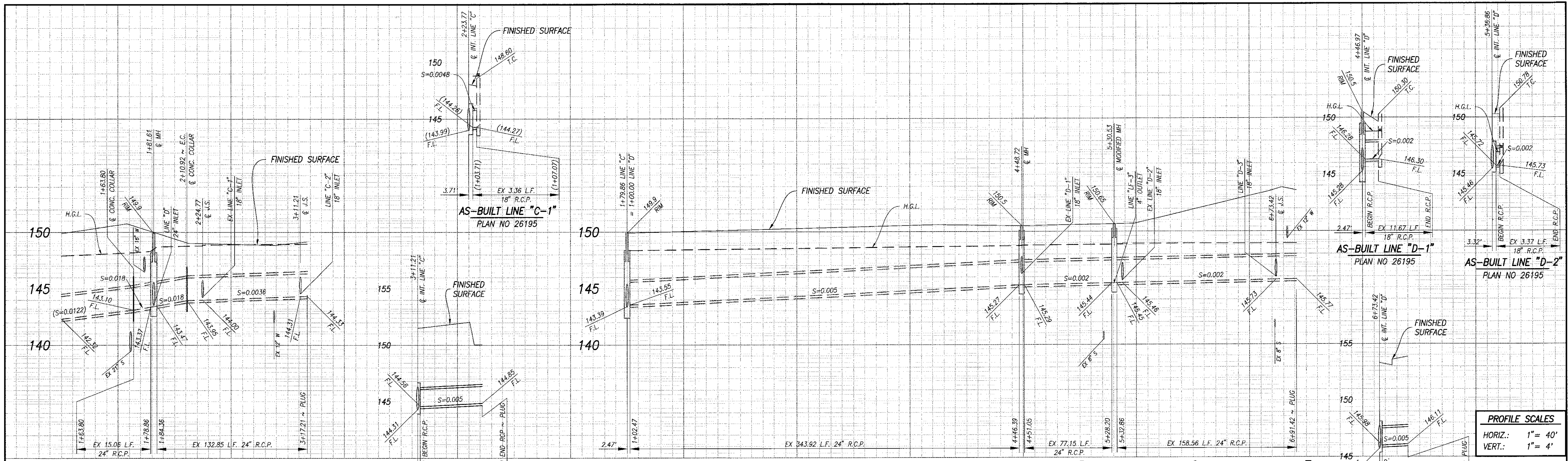
STORM DRAIN PLANS  
TRACT 17703

CITY OF ANAHEIM

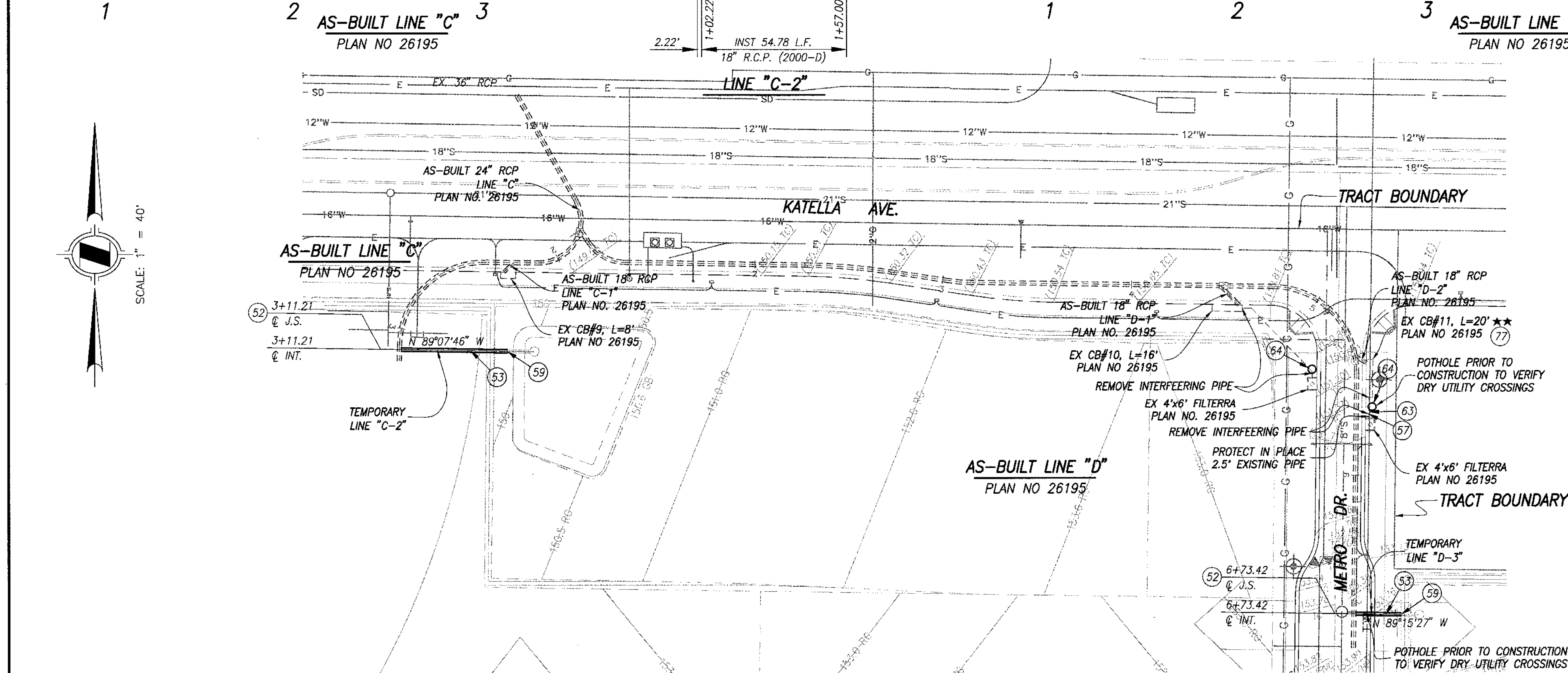
SHEET 1 OF 13

PLAN NO. 36204





**PROFILE SCALES**  
 HORIZ.: 1" = 40'  
 VERT.: 1" = 4'



**CONSTRUCTION NOTES**

- 52 CONST. J.S. PER SPPWC STD. PLAN NO. 331-3
- 53 INST. 18" R.C.P. (SEE PROFILE FOR D-LOAD) BEDDING PER OCPW STD. NO. 1319, DETAIL ON SHEET 13
- 57 INST. 22.5" ELBOW
- 59 CONST. DOUBLE BRICK AND MORTAR PLUG
- 63 INST. 4" SCH-80 PVC OUTLET PIPE
- 64 CONST. THE MAXWELL IV PER TORRENT RESOURCES, DETAIL ON SHEET 13
- 77 CONSTRUCT AUTOMATIC RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN ON EX. CATCH BASIN ★★

★★ INSTALL AUTOMATIC RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN, RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN SHALL BE CONSTRUCTED OF CORROSION RESISTANT MATERIALS AND SHALL BE "FULL CAPTURE" DESIGN AND OF MAINTAINABLE DESIGN. CONTRACTOR SHALL MAKE PRODUCT SUBMITTAL TO ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION.

**HYDRAULIC DATA**

LINE	STA to STA	Q <sub>10</sub>	DIA	S <sub>o</sub>	n	D <sub>c</sub>	V <sub>c</sub>	S <sub>c</sub>	D <sub>n</sub>	V <sub>n</sub>	V <sub>f</sub>	S <sub>f</sub>
"C"	1+00.00 1+63.80	15.1	24"	0.0122	0.013	1.39	6.37	0.0063	1.11	8.29	4.71	0.0043
"C"	1+63.80 1+78.86	15.1	24"	0.0180	0.013	1.39	6.37	0.0063	0.99	9.60	4.71	0.0043
"C"	1+84.36 2+10.92	8.8	24"	0.0180	0.013	0.76	4.27	0.0045	0.53	7.01	1.50	0.0004
"C"	2+10.92 2+24.77	8.8	24"	0.0036	0.013	0.67	3.98	0.0045	0.71	3.68	1.18	0.0003
"C"	2+24.77 3+09.21	7.1	24"	0.0036	0.013	0.95	4.85	0.0048	1.03	4.37	2.26	0.0010
"C"	3+09.21 4+04.92	0.0	24"	0.0036	0.013	0.00	0.00	0.0000	0.00	0.00	0.00	0.0000
"C-1"	---	1.9	18"	0.0048	0.013	0.43	3.14	0.0049	0.43	3.12	0.74	0.0002
"D"	1+02.47 4+46.39	7.4	24"	0.0050	0.013	1.12	5.42	0.0052	1.13	5.35	3.12	0.0019
"D"	4+51.05 5+37.72	6.5	24"	0.0020	0.013	0.74	4.19	0.0045	0.92	3.11	1.40	0.0004
"D"	5+37.72 6+91.42	0.00	24"	0.0020	0.013	0.00	0.00	0.0000	0.00	0.00	0.00	0.0000
"D-1"	---	1.1	18"	0.0020	0.013	0.39	3.00	0.0049	0.49	2.17	0.62	0.0001
"D-2"	---	6.5	18"	0.0020	0.013	0.99	5.28	0.0065	FULL	---	3.68	0.0038

THESE PLANS HAVE BEEN EXAMINED AND IS APPROVED ONLY AS TO COMPATIBILITY WITH ADJOINING EXISTING OR FUTURE IMPROVEMENTS AND CONFORMANCE WITH CITY OF ANAHEIM STANDARD DETAILS AND THE REQUIREMENTS FOR THE FOLLOWING APPLICABLE FACTORS: RIGHT-OF-WAY, ROADWAY MATERIALS, ALIGNMENTS AND GRADES, HYDROLOGY AND HYDRAULIC DESIGN OF STORMDRAIN OR SANITARY SEWER SYSTEMS AND UNDER GROUND CONDUIT OR OPEN CHANNEL CHANNEL ALIGNMENTS, GRADES, SIZES AND MATERIALS.

ENGINEER'S NOTE TO CONTRACTOR : THE EXISTENCE LOCATION OF ANY UNDERGROUND UTILITIES, PIPES, AND/OR STRUCTURES SHOWN ON THESE PLANS WERE OBTAINED BY A SEARCH OF AVAILABLE RECORDS. TO THE BEST OF OUR KNOWLEDGE, THERE ARE NO EXISTING UTILITIES EXCEPT AS SHOWN ON THESE PLANS. THE CONTRACTOR SHALL AS CERTAIN THE TRUE VERTICAL AND HORIZONTAL LOCATION AND SIZE OF THOSE TO BE USED OF ANY UNDERGROUND UTILITIES AND SHALL BE RESPONSIBLE FOR DAMAGE TO ANY PUBLIC OR PRIVATE UTILITIES AS SHOWN HEREON.

**REFERENCES**

NO.	INIT.	DATE	DESCRIPTION	DATE	APP'D

**APPROVAL**

BENCH MARK: 9A-22 ELEVATION: 151.99 (NAVD88)  
 KATELLA AVENUE/STATE COLLEGE BLVD.  
 BRASS CAP MKD. C OF A BM, IN THE TOP OF CURB AT THE SE COR.  
 ELEVATION: 151.99 (NAVD88)

PLANS FOR THESE IMPROVEMENTS: STREET: WATER: W-3175  
 SEWER: 36168-36170  
 STORM DRAIN: 36204-36216  
 LANDSCAPE:

FOR APPROVAL, SEE PLAN NO. 36204

ENGINEER: **HUNSAKER & ASSOCIATES**  
 IRVINE, INC.  
 PLANNING ■ ENGINEERING ■ SURVEYING  
 Three Hughes Irvine, CA 92618  
 FX: (949) 583-0759 PH: (949) 583-1010

*Ed Mandich* 5-6-16  
 EDWARD A. MANDICH, RCE NO. 59089 DATE

RCP 2015-11013

OWNER: **PT METRO, LLC**  
 25 ENTERPRISE, 3RD FLOOR  
 IRVINE, CA 92616  
 (949) 349-8000

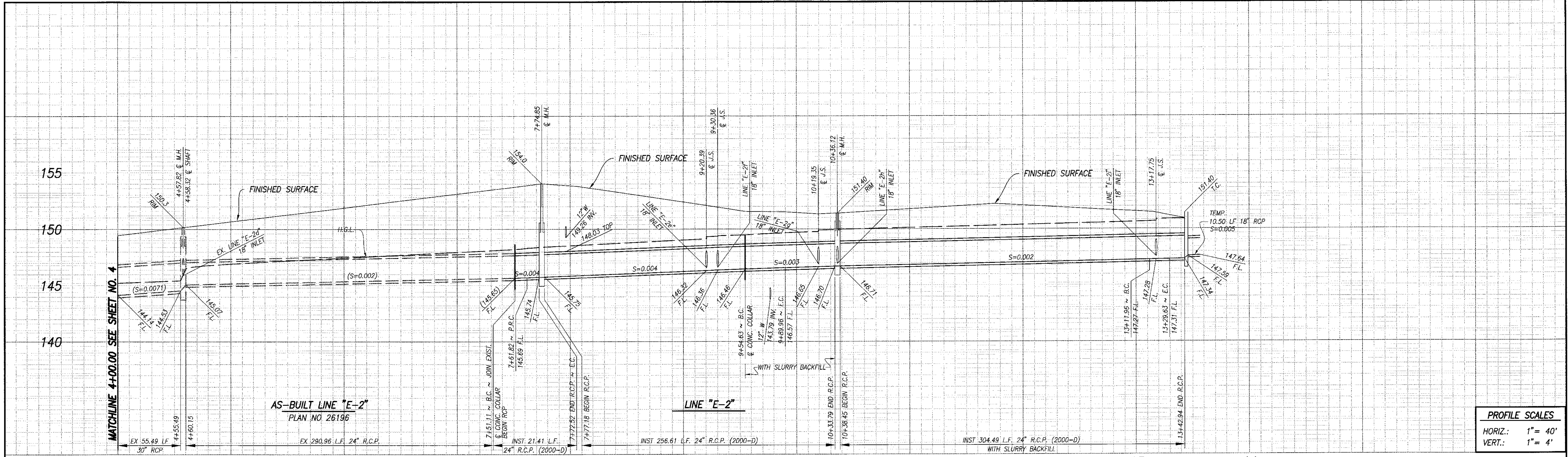
SOILS ENGINEER: **GROUP DELTA CONSULTANTS**  
 32 MAULCHLY, SUITE B  
 IRVINE, CA 92618  
 PH: (949) 450-2100

**STORM DRAIN PLANS**  
**TRACT 17703**  
 AS-BUILT LINES "C" AND "D"

CITY OF ANAHEIM

SHEET **3** OF **13**

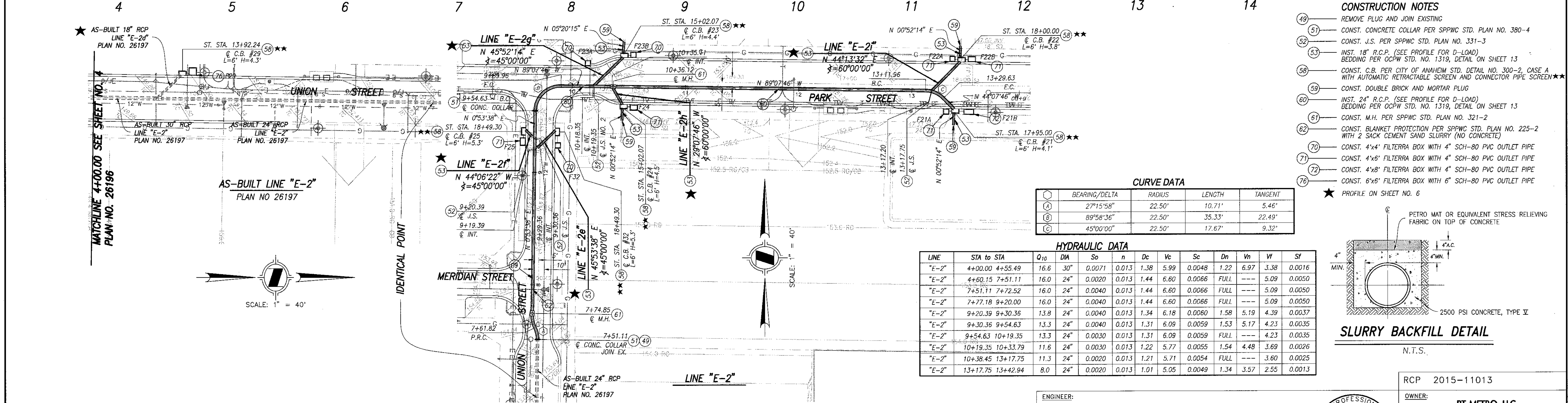
PLAN NO. **36206**



**PROFILE SCALES**

HORIZ.: 1" = 40'

VERT.: 1" = 4'



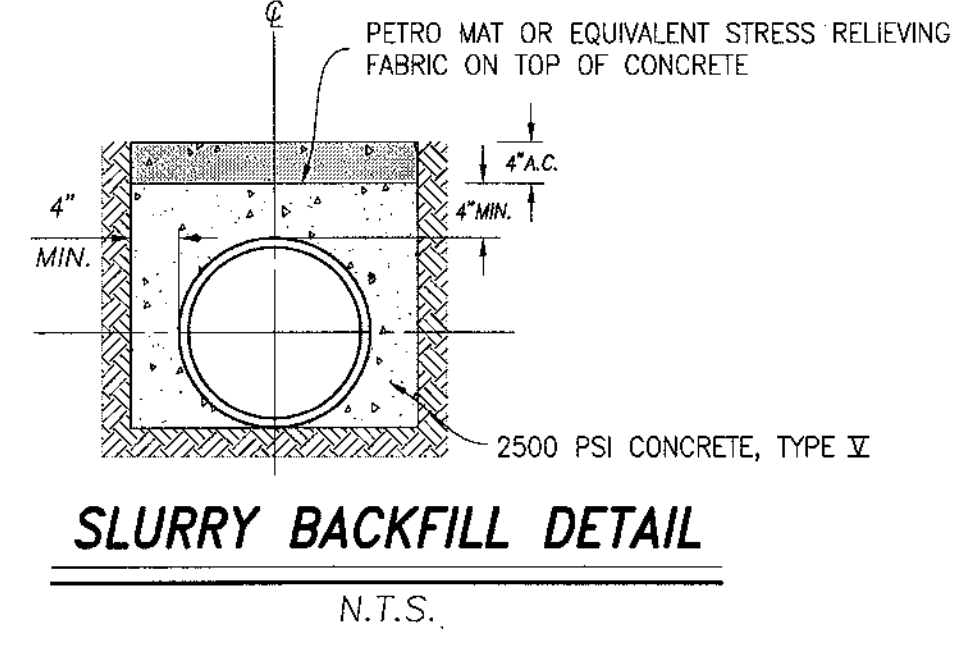
- CONSTRUCTION NOTES**
- 49 REMOVE PLUG AND JOIN EXISTING
  - 51 CONST. CONCRETE COLLAR PER SPPWC STD. PLAN NO. 380-4
  - 52 CONST. J.S. PER SPPWC STD. PLAN NO. 331-3
  - 53 INST. 18" R.C.P. (SEE PROFILE FOR D-LOAD) BEDDING PER OCPW STD. NO. 1319, DETAIL ON SHEET 13
  - 58 CONST. C.B. PER CITY OF ANAHEIM STD. DETAIL NO. 300-2, CASE A WITH AUTOMATIC RETRACTABLE SCREEN AND CONNECTOR PIPE SCREEN
  - 59 CONST. DOUBLE BRICK AND MORTAR PLUG
  - 60 INST. 24" R.C.P. (SEE PROFILE FOR D-LOAD) BEDDING PER OCPW STD. NO. 1319, DETAIL ON SHEET 13
  - 61 CONST. M.H. PER SPPWC STD. PLAN NO. 321-2
  - 62 CONST. BLANKET PROTECTION PER SPPWC STD. PLAN NO. 225-2 WITH 2 SACK CEMENT SAND SLURRY (NO CONCRETE)
  - 70 CONST. 4'x4' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE
  - 71 CONST. 4'x6' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE
  - 72 CONST. 4'x8' FILTERRA BOX WITH 4" SCH-80 PVC OUTLET PIPE
  - 76 CONST. 6'x6' FILTERRA BOX WITH 6" SCH-80 PVC OUTLET PIPE
- ★ PROFILE ON SHEET NO. 6

**CURVE DATA**

BEARING/DELTA	RADIUS	LENGTH	TANGENT
27°15'58"	22.50'	10.71'	5.46'
89°58'36"	22.50'	35.33'	22.49'
45°00'00"	22.50'	17.67'	9.32'

**HYDRAULIC DATA**

LINE	STA TO STA	Q <sub>10</sub>	DIA	S <sub>o</sub>	n	D <sub>c</sub>	V <sub>c</sub>	S <sub>c</sub>	D <sub>n</sub>	V <sub>n</sub>	V <sub>f</sub>	S <sub>f</sub>
"E-2"	4+00.00 4+55.49	16.6	30"	0.0071	0.013	1.38	5.99	0.0048	1.22	6.97	3.38	0.0016
"E-2"	4+60.15 7+51.11	16.0	24"	0.0020	0.013	1.44	6.60	0.0066	FULL	---	5.09	0.0050
"E-2"	7+51.11 7+72.52	16.0	24"	0.0040	0.013	1.44	6.60	0.0066	FULL	---	5.09	0.0050
"E-2"	7+72.52 9+20.00	16.0	24"	0.0040	0.013	1.44	6.60	0.0066	FULL	---	5.09	0.0050
"E-2"	9+20.00 9+30.36	13.8	24"	0.0040	0.013	1.34	6.18	0.0060	1.58	5.19	4.39	0.0037
"E-2"	9+30.36 9+54.63	13.3	24"	0.0040	0.013	1.31	6.09	0.0059	1.53	5.17	4.23	0.0035
"E-2"	9+54.63 10+19.35	13.3	24"	0.0030	0.013	1.31	6.09	0.0059	FULL	---	4.23	0.0035
"E-2"	10+19.35 10+33.79	11.6	24"	0.0030	0.013	1.22	5.77	0.0055	1.54	4.48	3.69	0.0026
"E-2"	10+33.79 13+17.75	11.3	24"	0.0020	0.013	1.21	5.71	0.0054	FULL	---	3.60	0.0025
"E-2"	13+17.75 13+42.94	8.0	24"	0.0020	0.013	1.01	5.05	0.0049	1.34	3.57	2.55	0.0013



THESE PLANS HAVE BEEN EXAMINED AND IS APPROVED ONLY AS TO COMPATIBILITY WITH ADJOINING EXISTING OR FUTURE IMPROVEMENTS AND CONFORMANCE WITH CITY OF ANAHEIM STANDARD DETAILS AND THE REQUIREMENTS FOR THE FOLLOWING APPLICABLE FACTORS: RIGHT-OF-WAY, ROADWAY MATERIALS, ALIGNMENTS AND GRADES, HYDROLOGY AND HYDRAULIC DESIGN OF STORMDRAIN OR SANITARY SEWER SYSTEMS AND UNDER GROUND CONDUIT OR OPEN CHANNEL CHANNEL ALIGNMENTS, GRADES, SIZES AND MATERIALS.

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ENGINEER: **HUNSAKER & ASSOCIATES IRVINE, INC.**

PLANNING ■ ENGINEERING ■ SURVEYING

Three Hughes ■ Irvine, CA 92618

FX: (949) 583-0759 ■ PH: (949) 583-1010

EDWARD A. MANDICH, RCE NO. 59089

PT METRO, LLC  
25 ENTERPRISE, 3rd FLOOR  
ALISO VIEJO, CA 92656  
(949) 349-8000

SOILS ENGINEER: **GROUP DELTA CONSULTANTS**  
32 MAULCHLY, SUITE B  
IRVINE, CA 92618  
PH: (949) 450-2100

**REVISIONS**

NO.	INIT.	DATE	DESCRIPTION	DATE	APP'D

**REFERENCES**

BENCH MARK: 9A-22 ELEVATION: 151.99 (NAVD88)

KATELLA AVENUE/STATE COLLEGE BLVD. BRASS CAP MKD C OF A BM, IN THE TOP OF CURB AT THE SE COR. ELEVATION: 151.99 (NAVD88)

PLANS FOR THESE IMPROVEMENTS: STREET: WATER: W-3175

SEWER: 36168-36170

STORM DRAIN: 36204-36216

LANDSCAPE:

**APPROVAL**

FOR APPROVAL, SEE PLAN NO. 36204

**STORM DRAIN PLANS TRACT 17703**

LINE "E-2" EXTENSION

CITY OF ANAHEIM

SHEET 5 OF 13

PLAN NO. 36208

PLOTTED BY: Tiffany Nguyen DATE: Apr. 27, 2016 03:21:03 PM FILE: F:\0108\Engineering\TR\_17703\Imp\_Storm Drain\SH-05.dwg

D-108  
36208  
FOR CITY W/O 3816-14 STORM DRAIN IMPROVEMENT PLANS  
USE ONLY ROOM: 74016  
DOC: 74016

**APPROVED**  
**HYDROLOGY CALCS AND MAP**  
**FOR A-TOWN TRACT 17703**

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2013 Advanced Engineering Software (aes)  
Ver. 20.0 Release Date: 06/01/2013 License ID 1239

Analysis prepared by:

HUNSAKER & ASSOCIATES  
Irvine, Inc  
Planning \* Engineering \* Surveying  
Three Hughes \* Irvine, California 92618 \* (949)583-1010

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* W.O. #1855-150, A-TOWN METRO \*  
\* 10-YR STUDY \*  
\* PROPOSED CONDITION \*  
\*\*\*\*\*

FILE NAME: 17703.DAT  
TIME/DATE OF STUDY: 20:01 03/23/2015

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL IN- / OUT- / PARK- SIDE / SIDE/ WAY	CURB GUTTER-GEOMETRIES: HEIGHT (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

-----

INITIAL SUBAREA FLOW-LENGTH(FEET) = 230.00  
ELEVATION DATA: UPSTREAM(FEET) = 151.75 DOWNSTREAM(FEET) = 149.08

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.525  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.485  
SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.20	0.40	0.100	32	6.53

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA RUNOFF(CFS) = 0.62  
TOTAL AREA(ACRES) = 0.20 PEAK FLOW RATE(CFS) = 0.62

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 61

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 149.08 DOWNSTREAM ELEVATION(FEET) = 148.38  
STREET LENGTH(FEET) = 133.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 21.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 16.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.21  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.38  
HALFSTREET FLOOD WIDTH(FEET) = 12.66  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.86  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.71  
STREET FLOW TRAVEL TIME(MIN.) = 1.19 Tc(MIN.) = 7.71  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.166

SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
APARTMENTS	A	1.86	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA AREA(ACRES) = 1.86 SUBAREA RUNOFF(CFS) = 5.17  
EFFECTIVE AREA(ACRES) = 2.06 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 5.73

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 15.97  
FLOW VELOCITY(FEET/SEC.) = 2.15 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.96  
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 363.00 FEET.

```

*****
FLOW PROCESS FROM NODE      3.00 TO NODE      7.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 143.24  DOWNSTREAM(FEET) = 143.15
FLOW LENGTH(FEET) = 41.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.26
ESTIMATED PIPE DIAMETER(INCH) = 21.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.73
PIPE TRAVEL TIME(MIN.) = 0.21  Tc(MIN.) = 7.92
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 7.00 = 404.00 FEET.

*****
FLOW PROCESS FROM NODE      7.00 TO NODE      7.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 7.92
RAINFALL INTENSITY(INCH/HR) = 3.12
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.19
EFFECTIVE STREAM AREA(ACRES) = 2.06
TOTAL STREAM AREA(ACRES) = 2.06
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.73

*****
FLOW PROCESS FROM NODE      4.00 TO NODE      5.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 235.00
ELEVATION DATA: UPSTREAM(FEET) = 151.75  DOWNSTREAM(FEET) = 149.08

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.610
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.459
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/  SCS SOIL  AREA  Fp  Ap  SCS  Tc
LAND USE  GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
COMMERCIAL  A  0.21  0.40  0.100  32  6.61
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 0.65
TOTAL AREA(ACRES) = 0.21  PEAK FLOW RATE(CFS) = 0.65

*****
FLOW PROCESS FROM NODE      5.00 TO NODE      6.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

```

```

>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 149.08  DOWNSTREAM ELEVATION(FEET) = 147.65
STREET LENGTH(FEET) = 185.00  CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 21.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 16.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.87
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 6.53
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.60
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.41
STREET FLOW TRAVEL TIME(MIN.) = 1.93  Tc(MIN.) = 8.54
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.988
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/  SCS SOIL  AREA  Fp  Ap  SCS
LAND USE  GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL  A  0.17  0.40  0.100  32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.17  SUBAREA RUNOFF(CFS) = 0.45
EFFECTIVE AREA(ACRES) = 0.38  AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.40  AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 0.4  PEAK FLOW RATE(CFS) = 1.01

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.27  HALFSTREET FLOOD WIDTH(FEET) = 6.97
FLOW VELOCITY(FEET/SEC.) = 1.67  DEPTH*VELOCITY(FT*FT/SEC.) = 0.44
LONGEST FLOWPATH FROM NODE 4.00 TO NODE 6.00 = 420.00 FEET.

*****
FLOW PROCESS FROM NODE      6.00 TO NODE      6.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 8.54
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.988
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/  SCS SOIL  AREA  Fp  Ap  SCS
LAND USE  GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
APARTMENTS  A  1.76  0.40  0.200  32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 1.76  SUBAREA RUNOFF(CFS) = 4.61
EFFECTIVE AREA(ACRES) = 2.14  AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.40  AREA-AVERAGED Ap = 0.18
TOTAL AREA(ACRES) = 2.1  PEAK FLOW RATE(CFS) = 5.61

```

```

*****
FLOW PROCESS FROM NODE      6.00 TO NODE      6.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc (MIN.) =      8.54
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.988
SUBAREA LOSS RATE DATA (AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE                GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL              A      0.38    0.40    0.100    32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 0.38      SUBAREA RUNOFF (CFS) = 1.01
EFFECTIVE AREA (ACRES) = 2.52    AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.17
TOTAL AREA (ACRES) = 2.5        PEAK FLOW RATE (CFS) = 6.62

*****
FLOW PROCESS FROM NODE      6.00 TO NODE      7.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM (FEET) = 143.49 DOWNSTREAM (FEET) = 143.15
FLOW LENGTH (FEET) = 13.50 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER (INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.1 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 8.55
ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 6.62
PIPE TRAVEL TIME (MIN.) = 0.03 Tc (MIN.) = 8.56
LONGEST FLOWPATH FROM NODE 4.00 TO NODE 7.00 = 433.50 FEET.

*****
FLOW PROCESS FROM NODE      7.00 TO NODE      7.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION (MIN.) = 8.56
RAINFALL INTENSITY (INCH/HR) = 2.98
AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.17
EFFECTIVE STREAM AREA (ACRES) = 2.52
TOTAL STREAM AREA (ACRES) = 2.52
PEAK FLOW RATE (CFS) AT CONFLUENCE = 6.62

** CONFLUENCE DATA **
STREAM      Q      Tc      Intensity  Fp (Fm)      Ap      Ae      HEADWATER
NUMBER      (CFS) (MIN.) (INCH/HR) (INCH/HR) (INCH/HR) (ACRES) NODE
1           5.73  7.92  3.118  0.40 (0.08) 0.19  2.1    1.00

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```

2           6.62  8.56  2.983  0.40 (0.07) 0.17  2.5    4.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      Q      Tc      Intensity  Fp (Fm)      Ap      Ae      HEADWATER
NUMBER      (CFS) (MIN.) (INCH/HR) (INCH/HR) (INCH/HR) (ACRES) NODE
1           12.14  7.92  3.118  0.40 (0.07) 0.18  4.4    1.00
2           12.10  8.56  2.983  0.40 (0.07) 0.18  4.6    4.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE (CFS) = 12.14 Tc (MIN.) = 7.92
EFFECTIVE AREA (ACRES) = 4.39 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.18
TOTAL AREA (ACRES) = 4.6
LONGEST FLOWPATH FROM NODE 4.00 TO NODE 7.00 = 433.50 FEET.

*****
FLOW PROCESS FROM NODE      7.00 TO NODE      8.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM (FEET) = 143.15 DOWNSTREAM (FEET) = 143.04
FLOW LENGTH (FEET) = 55.80 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.6 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 3.73
ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 12.14
PIPE TRAVEL TIME (MIN.) = 0.25 Tc (MIN.) = 8.17
LONGEST FLOWPATH FROM NODE 4.00 TO NODE 8.00 = 489.30 FEET.

*****
FLOW PROCESS FROM NODE      8.00 TO NODE      8.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc (MIN.) = 8.17
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.063
SUBAREA LOSS RATE DATA (AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE                GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL              A      0.66    0.40    0.100    32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 0.66      SUBAREA RUNOFF (CFS) = 1.80
EFFECTIVE AREA (ACRES) = 5.05    AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.17
TOTAL AREA (ACRES) = 5.2        PEAK FLOW RATE (CFS) = 13.62

*****
FLOW PROCESS FROM NODE      11.00 TO NODE     12.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

```

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
 ELEVATION DATA: UPSTREAM (FEET) = 152.08 DOWNSTREAM (FEET) = 148.28

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.132  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.312  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.35	0.40	0.100	32	7.13

SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF (CFS) = 1.03  
 TOTAL AREA (ACRES) = 0.35 PEAK FLOW RATE (CFS) = 1.03

\*\*\*\*\*

FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 61

-----

>>>> COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA <<<<<  
 >>>> (STANDARD CURB SECTION USED) <<<<<

=====

UPSTREAM ELEVATION (FEET) = 148.28 DOWNSTREAM ELEVATION (FEET) = 147.40  
 STREET LENGTH (FEET) = 113.00 CURB HEIGHT (INCHES) = 6.0  
 STREET HALFWIDTH (FEET) = 24.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 19.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 1.38  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.29  
 HALFSTREET FLOOD WIDTH (FEET) = 8.08  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 1.80  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.52  
 STREET FLOW TRAVEL TIME (MIN.) = 1.05 Tc (MIN.) = 8.18  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.062  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.26	0.40	0.100	32

SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.26 SUBAREA RUNOFF (CFS) = 0.71  
 EFFECTIVE AREA (ACRES) = 0.61 AREA-AVERAGED Fm (INCH/HR) = 0.04  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA (ACRES) = 0.6 PEAK FLOW RATE (CFS) = 1.66

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.30 HALFSTREET FLOOD WIDTH (FEET) = 8.82

FLOW VELOCITY (FEET/SEC.) = 1.85 DEPTH\*VELOCITY (FT\*FT/SEC.) = 0.56  
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 13.00 = 413.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 13.00 TO NODE 13.00 IS CODE = 81

-----

>>>> ADDITION OF SUBAREA TO MAINLINE PEAK FLOW <<<<<

=====

MAINLINE Tc (MIN.) = 8.18  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.062  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
APARTMENTS	A	1.96	0.40	0.200	32

SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA AREA (ACRES) = 1.96 SUBAREA RUNOFF (CFS) = 5.26  
 EFFECTIVE AREA (ACRES) = 2.57 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.18  
 TOTAL AREA (ACRES) = 2.6 PEAK FLOW RATE (CFS) = 6.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 13.00 TO NODE 14.00 IS CODE = 31

-----

>>>> COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA <<<<<  
 >>>> USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 143.21 DOWNSTREAM (FEET) = 143.15  
 FLOW LENGTH (FEET) = 28.60 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 14.9 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.39  
 ESTIMATED PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 6.92  
 PIPE TRAVEL TIME (MIN.) = 0.14 Tc (MIN.) = 8.32  
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 14.00 = 441.60 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 81

-----

>>>> ADDITION OF SUBAREA TO MAINLINE PEAK FLOW <<<<<

=====

MAINLINE Tc (MIN.) = 8.32  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.032  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.77	0.40	0.100	32

SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.77 SUBAREA RUNOFF (CFS) = 2.07  
 EFFECTIVE AREA (ACRES) = 3.34 AREA-AVERAGED Fm (INCH/HR) = 0.06  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.16  
 TOTAL AREA (ACRES) = 3.3 PEAK FLOW RATE (CFS) = 8.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
 -----

INITIAL SUBAREA FLOW-LENGTH (FEET) = 245.00  
 ELEVATION DATA: UPSTREAM (FEET) = 154.00 DOWNSTREAM (FEET) = 151.70

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.442  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.232  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	A	0.66	0.40	0.200	32	7.44

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF (CFS) = 1.87  
 TOTAL AREA (ACRES) = 0.66 PEAK FLOW RATE (CFS) = 1.87

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<  
 -----

UPSTREAM ELEVATION (FEET) = 151.70 DOWNSTREAM ELEVATION (FEET) = 150.90  
 STREET LENGTH (FEET) = 325.00 CURB HEIGHT (INCHES) = 6.0  
 STREET HALFWIDTH (FEET) = 15.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 10.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 4.37  
 \*\*\*STREET FLOW SPLITS OVER STREET-CROWN\*\*\*  
 FULL DEPTH (FEET) = 0.43 FLOOD WIDTH (FEET) = 15.00  
 FULL HALF-STREET VELOCITY (FEET/SEC.) = 1.41  
 SPLIT DEPTH (FEET) = 0.31 SPLIT FLOOD WIDTH (FEET) = 9.26  
 SPLIT FLOW (CFS) = 1.04 SPLIT VELOCITY (FEET/SEC.) = 1.06  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.43  
 HALFSTREET FLOOD WIDTH (FEET) = 15.00  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 1.41  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.60  
 STREET FLOW TRAVEL TIME (MIN.) = 3.85 Tc (MIN.) = 11.29  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.545

SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
APARTMENTS	A	2.25	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA AREA (ACRES) = 2.25 SUBAREA RUNOFF (CFS) = 4.99  
 EFFECTIVE AREA (ACRES) = 2.91 AREA-AVERAGED Fm (INCH/HR) = 0.08  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA (ACRES) = 2.9 PEAK FLOW RATE (CFS) = 6.46

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.43 HALFSTREET FLOOD WIDTH (FEET) = 15.00  
 FLOW VELOCITY (FEET/SEC.) = 1.41 DEPTH\*VELOCITY (FT\*FT/SEC.) = 0.60  
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 570.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 -----

ELEVATION DATA: UPSTREAM (FEET) = 145.49 DOWNSTREAM (FEET) = 145.28  
 FLOW LENGTH (FEET) = 89.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.3 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.43  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 6.46  
 PIPE TRAVEL TIME (MIN.) = 0.43 Tc (MIN.) = 11.73  
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 24.00 = 659.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 24.00 TO NODE 24.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 -----

MAINLINE Tc (MIN.) = 11.73  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.491  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.48	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.48 SUBAREA RUNOFF (CFS) = 1.06  
 EFFECTIVE AREA (ACRES) = 3.39 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
 TOTAL AREA (ACRES) = 3.4 PEAK FLOW RATE (CFS) = 7.37

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 24.00 TO NODE 30.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 -----

ELEVATION DATA: UPSTREAM (FEET) = 145.28 DOWNSTREAM (FEET) = 143.40  
 FLOW LENGTH (FEET) = 348.60 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.6 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.91  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 7.37



PIPE TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 12.91  
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 30.00 = 1007.60 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 30.00 TO NODE 30.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.91  
 RAINFALL INTENSITY(INCH/HR) = 2.36  
 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.19  
 EFFECTIVE STREAM AREA(ACRES) = 3.39  
 TOTAL STREAM AREA(ACRES) = 3.39  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.37

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 25.00 TO NODE 26.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
 =====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 250.00  
 ELEVATION DATA: UPSTREAM(FEET) = 153.50 DOWNSTREAM(FEET) = 151.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.408  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.241  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	A	0.60	0.40	0.200	32	7.41

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF(CFS) = 1.71  
 TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 26.00 TO NODE 27.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 151.00 DOWNSTREAM(FEET) = 150.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 110.00 CHANNEL SLOPE = 0.0091  
 CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 5.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.076  
 SUBAREA LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
APARTMENTS	A	0.56	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.46  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.60  
 AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 0.71  
 Tc(MIN.) = 8.11  
 SUBAREA AREA(ACRES) = 0.56 SUBAREA RUNOFF(CFS) = 1.51  
 EFFECTIVE AREA(ACRES) = 1.16 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 3.13

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.19 FLOW VELOCITY(FEET/SEC.) = 2.80  
 LONGEST FLOWPATH FROM NODE 25.00 TO NODE 27.00 = 360.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 27.00 TO NODE 28.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 144.50 DOWNSTREAM(FEET) = 144.30  
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.14  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.13  
 PIPE TRAVEL TIME(MIN.) = 0.37 Tc(MIN.) = 8.49  
 LONGEST FLOWPATH FROM NODE 25.00 TO NODE 28.00 = 430.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 28.00 TO NODE 28.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<  
 =====

MAINLINE Tc(MIN.) = 8.49  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.998  
 SUBAREA LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
APARTMENTS	A	1.54	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA AREA(ACRES) = 1.54 SUBAREA RUNOFF(CFS) = 4.04  
 EFFECTIVE AREA(ACRES) = 2.70 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 7.09

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 28.00 TO NODE 29.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 144.30 DOWNSTREAM(FEET) = 144.00  
 FLOW LENGTH(FEET) = 85.40 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.2 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.11  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 7.09  
 PIPE TRAVEL TIME (MIN.) = 0.35 Tc (MIN.) = 8.83  
 LONGEST FLOWPATH FROM NODE 25.00 TO NODE 29.00 = 515.40 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

-----  
 MAINLINE Tc (MIN.) = 8.83  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.930  
 SUBAREA LOSS RATE DATA (AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL A 0.71 0.40 0.100 32  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.71 SUBAREA RUNOFF (CFS) = 1.85  
 EFFECTIVE AREA (ACRES) = 3.41 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.18  
 TOTAL AREA (ACRES) = 3.4 PEAK FLOW RATE (CFS) = 8.77

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 29.00 TO NODE 30.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

-----  
 ELEVATION DATA: UPSTREAM (FEET) = 144.00 DOWNSTREAM (FEET) = 143.40  
 FLOW LENGTH (FEET) = 43.20 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.6 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 7.28  
 ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 8.77  
 PIPE TRAVEL TIME (MIN.) = 0.10 Tc (MIN.) = 8.93  
 LONGEST FLOWPATH FROM NODE 25.00 TO NODE 30.00 = 558.60 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 30.00 TO NODE 30.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

-----  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 8.93  
 RAINFALL INTENSITY (INCH/HR) = 2.91  
 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.18  
 EFFECTIVE STREAM AREA (ACRES) = 3.41  
 TOTAL STREAM AREA (ACRES) = 3.41  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 8.77

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.37	12.91	2.358	0.40 (0.07)	0.19	3.4	21.00
2	8.77	8.93	2.911	0.40 (0.07)	0.18	3.4	25.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	15.11	8.93	2.911	0.40 (0.07)	0.18	5.8	25.00
2	14.43	12.91	2.358	0.40 (0.07)	0.18	6.8	21.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 15.11 Tc (MIN.) = 8.93  
 EFFECTIVE AREA (ACRES) = 5.76 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.18  
 TOTAL AREA (ACRES) = 6.8  
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 30.00 = 1007.60 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 31.00 TO NODE 32.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

-----  
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
 ELEVATION DATA: UPSTREAM (FEET) = 152.00 DOWNSTREAM (FEET) = 150.05

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)]\*\* 0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 12.948  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.353  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 PUBLIC PARK A 1.38 0.40 0.850 32 12.95  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850  
 SUBAREA RUNOFF (CFS) = 2.50  
 TOTAL AREA (ACRES) = 1.38 PEAK FLOW RATE (CFS) = 2.50

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 32.00 TO NODE 32.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

-----  
 MAINLINE Tc (MIN.) = 12.95  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.353  
 SUBAREA LOSS RATE DATA (AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL A 0.33 0.40 0.100 32  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 0.33 SUBAREA RUNOFF (CFS) = 0.69
EFFECTIVE AREA (ACRES) = 1.71 AREA-AVERAGED Fm (INCH/HR) = 0.28
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.71
TOTAL AREA (ACRES) = 1.7 PEAK FLOW RATE (CFS) = 3.19
*****
FLOW PROCESS FROM NODE 32.00 TO NODE 33.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
-----
ELEVATION DATA: UPSTREAM (FEET) = 142.10 DOWNSTREAM (FEET) = 141.80
FLOW LENGTH (FEET) = 172.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 2.59
ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 3.19
PIPE TRAVEL TIME (MIN.) = 1.11 Tc (MIN.) = 14.05
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 33.00 = 472.00 FEET.
*****
FLOW PROCESS FROM NODE 33.00 TO NODE 33.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
-----
MAINLINE Tc (MIN.) = 14.05
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.245
SUBAREA LOSS RATE DATA (AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.24 0.40 0.100 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 0.24 SUBAREA RUNOFF (CFS) = 0.48
EFFECTIVE AREA (ACRES) = 1.95 AREA-AVERAGED Fm (INCH/HR) = 0.25
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.63
TOTAL AREA (ACRES) = 2.0 PEAK FLOW RATE (CFS) = 3.50
*****
FLOW PROCESS FROM NODE 33.00 TO NODE 34.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
-----
ELEVATION DATA: UPSTREAM (FEET) = 141.80 DOWNSTREAM (FEET) = 141.77
FLOW LENGTH (FEET) = 6.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER (INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 3.98
ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 3.50
PIPE TRAVEL TIME (MIN.) = 0.03 Tc (MIN.) = 14.08
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 34.00 = 478.00 FEET.
*****

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FLOW PROCESS FROM NODE 34.00 TO NODE 34.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
-----
MAINLINE Tc (MIN.) = 14.08
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.243
SUBAREA LOSS RATE DATA (AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
APARTMENTS A 1.44 0.40 0.200 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA (ACRES) = 1.44 SUBAREA RUNOFF (CFS) = 2.80
EFFECTIVE AREA (ACRES) = 3.39 AREA-AVERAGED Fm (INCH/HR) = 0.18
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.45
TOTAL AREA (ACRES) = 3.4 PEAK FLOW RATE (CFS) = 6.30
*****
FLOW PROCESS FROM NODE 34.00 TO NODE 35.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
-----
ELEVATION DATA: UPSTREAM (FEET) = 141.77 DOWNSTREAM (FEET) = 141.72
FLOW LENGTH (FEET) = 34.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.7 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 2.89
ESTIMATED PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 6.30
PIPE TRAVEL TIME (MIN.) = 0.20 Tc (MIN.) = 14.28
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 35.00 = 512.00 FEET.
*****
FLOW PROCESS FROM NODE 35.00 TO NODE 35.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
-----
MAINLINE Tc (MIN.) = 14.28
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.225
SUBAREA LOSS RATE DATA (AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.39 0.40 0.100 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 0.39 SUBAREA RUNOFF (CFS) = 0.77
EFFECTIVE AREA (ACRES) = 3.78 AREA-AVERAGED Fm (INCH/HR) = 0.16
AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.41
TOTAL AREA (ACRES) = 3.8 PEAK FLOW RATE (CFS) = 7.01
*****
FLOW PROCESS FROM NODE 35.00 TO NODE 36.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
-----

```

ELEVATION DATA: UPSTREAM( FEET ) = 141.72 DOWNSTREAM( FEET ) = 141.12  
 FLOW LENGTH( FEET ) = 297.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.2 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC. ) = 3.35  
 ESTIMATED PIPE DIAMETER( INCH ) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS ) = 7.01  
 PIPE TRAVEL TIME( MIN. ) = 1.48 Tc( MIN. ) = 15.75  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 36.00 = 809.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 36.00 TO NODE 36.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION( MIN. ) = 15.75  
 RAINFALL INTENSITY( INCH/HR ) = 2.10  
 AREA-AVERAGED Fm( INCH/HR ) = 0.16  
 AREA-AVERAGED Fp( INCH/HR ) = 0.40  
 AREA-AVERAGED Ap = 0.41  
 EFFECTIVE STREAM AREA( ACRES ) = 3.78  
 TOTAL STREAM AREA( ACRES ) = 3.78  
 PEAK FLOW RATE( CFS ) AT CONFLUENCE = 7.01

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 35.10 TO NODE 36.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH( FEET ) = 246.00  
 ELEVATION DATA: UPSTREAM( FEET ) = 152.22 DOWNSTREAM( FEET ) = 150.75

Tc = K\*[ (LENGTH\*\* 3.00)/(ELEVATION CHANGE) ]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc( MIN. ) = 7.655  
 \* 10 YEAR RAINFALL INTENSITY( INCH/HR ) = 3.180  
 SUBAREA Tc AND LOSS RATE DATA( AMC II ):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.30	0.40	0.100	32	7.66

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp( INCH/HR ) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF( CFS ) = 0.85  
 TOTAL AREA( ACRES ) = 0.30 PEAK FLOW RATE( CFS ) = 0.85

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 36.00 TO NODE 36.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION( MIN. ) = 7.66  
 RAINFALL INTENSITY( INCH/HR ) = 3.18

AREA-AVERAGED Fm( INCH/HR ) = 0.04  
 AREA-AVERAGED Fp( INCH/HR ) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA( ACRES ) = 0.30  
 TOTAL STREAM AREA( ACRES ) = 0.30  
 PEAK FLOW RATE( CFS ) AT CONFLUENCE = 0.85

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.01	15.75	2.103	0.40( 0.16)	0.41	3.8	31.00
2	0.85	7.66	3.180	0.40( 0.04)	0.10	0.3	35.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.15	7.66	3.180	0.40( 0.15)	0.37	2.1	35.10
2	7.57	15.75	2.103	0.40( 0.16)	0.39	4.1	31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE( CFS ) = 7.57 Tc( MIN. ) = 15.75  
 EFFECTIVE AREA( ACRES ) = 4.08 AREA-AVERAGED Fm( INCH/HR ) = 0.16  
 AREA-AVERAGED Fp( INCH/HR ) = 0.40 AREA-AVERAGED Ap = 0.39  
 TOTAL AREA( ACRES ) = 4.1  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 36.00 = 809.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 36.00 TO NODE 37.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET ) = 141.12 DOWNSTREAM( FEET ) = 141.07  
 FLOW LENGTH( FEET ) = 15.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.2 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC. ) = 4.07  
 ESTIMATED PIPE DIAMETER( INCH ) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS ) = 7.57  
 PIPE TRAVEL TIME( MIN. ) = 0.06 Tc( MIN. ) = 15.82  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 37.00 = 824.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 37.00 TO NODE 37.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION( MIN. ) = 15.82  
 RAINFALL INTENSITY( INCH/HR ) = 2.10  
 AREA-AVERAGED Fm( INCH/HR ) = 0.16  
 AREA-AVERAGED Fp( INCH/HR ) = 0.40  
 AREA-AVERAGED Ap = 0.39

EFFECTIVE STREAM AREA (ACRES) = 4.08  
 TOTAL STREAM AREA (ACRES) = 4.08  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 7.57

2	6.68	7.73	3.163	0.40 ( 0.14)	0.35	2.3	36.10
3	7.92	15.82	2.099	0.40 ( 0.15)	0.38	4.3	31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 7.92 Tc (MIN.) = 15.82  
 EFFECTIVE AREA (ACRES) = 4.27 AREA-AVERAGED Fm (INCH/HR) = 0.15  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.38  
 TOTAL AREA (ACRES) = 4.3  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 37.00 = 824.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 36.10 TO NODE 37.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 250.00  
 ELEVATION DATA: UPSTREAM (FEET) = 152.22 DOWNSTREAM (FEET) = 150.75

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.730  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.163  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.19	0.40	0.100	32	7.73

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF (CFS) = 0.53  
 TOTAL AREA (ACRES) = 0.19 PEAK FLOW RATE (CFS) = 0.53

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 37.00 TO NODE 37.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 7.73  
 RAINFALL INTENSITY (INCH/HR) = 3.16  
 AREA-AVERAGED Fm (INCH/HR) = 0.04  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA (ACRES) = 0.19  
 TOTAL STREAM AREA (ACRES) = 0.19  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 0.53

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.15	7.72	3.165	0.40 ( 0.15)	0.37	2.1	35.10
1	7.57	15.82	2.099	0.40 ( 0.16)	0.39	4.1	31.00
2	0.53	7.73	3.163	0.40 ( 0.04)	0.10	0.2	36.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.68	7.72	3.165	0.40 ( 0.14)	0.35	2.3	35.10

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 37.00 TO NODE 38.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 141.07 DOWNSTREAM (FEET) = 140.67  
 FLOW LENGTH (FEET) = 136.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.7 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.86  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 7.92  
 PIPE TRAVEL TIME (MIN.) = 0.59 Tc (MIN.) = 16.40  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 38.00 = 960.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 38.00 TO NODE 38.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 16.40  
 RAINFALL INTENSITY (INCH/HR) = 2.06  
 AREA-AVERAGED Fm (INCH/HR) = 0.15  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.38  
 EFFECTIVE STREAM AREA (ACRES) = 4.27  
 TOTAL STREAM AREA (ACRES) = 4.27  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 7.92

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 37.10 TO NODE 38.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
 ELEVATION DATA: UPSTREAM (FEET) = 148.90 DOWNSTREAM (FEET) = 145.59

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.814  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.143  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)

APARTMENTS A 0.73 0.40 0.200 32 7.81  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF(CFS) = 2.01  
 TOTAL AREA(ACRES) = 0.73 PEAK FLOW RATE(CFS) = 2.01

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 38.00 TO NODE 38.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.81  
 RAINFALL INTENSITY(INCH/HR) = 3.14  
 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.20  
 EFFECTIVE STREAM AREA(ACRES) = 0.73  
 TOTAL STREAM AREA(ACRES) = 0.73  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.01

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.68	8.32	3.032	0.40( 0.14)	0.35	2.3	35.10
1	6.68	8.33	3.030	0.40( 0.14)	0.35	2.3	36.10
1	7.92	16.40	2.055	0.40( 0.15)	0.38	4.3	31.00
2	2.01	7.81	3.143	0.40( 0.08)	0.20	0.7	37.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.53	7.81	3.143	0.40( 0.12)	0.31	2.9	37.10
2	8.62	8.32	3.032	0.40( 0.12)	0.31	3.1	35.10
3	8.62	8.33	3.030	0.40( 0.12)	0.31	3.1	36.10
4	9.22	16.40	2.055	0.40( 0.14)	0.35	5.0	31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 9.22 Tc(MIN.) = 16.40  
 EFFECTIVE AREA(ACRES) = 5.00 AREA-AVERAGED Fm(INCH/HR) = 0.14  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.35  
 TOTAL AREA(ACRES) = 5.0  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 38.00 = 960.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 38.00 TO NODE 39.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 140.67 DOWNSTREAM(FEET) = 140.12

FLOW LENGTH(FEET) = 99.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.20  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 9.22  
 PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 16.72  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 39.00 = 1059.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 39.00 TO NODE 39.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 16.72  
 RAINFALL INTENSITY(INCH/HR) = 2.03  
 AREA-AVERAGED Fm(INCH/HR) = 0.14  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.35  
 EFFECTIVE STREAM AREA(ACRES) = 5.00  
 TOTAL STREAM AREA(ACRES) = 5.00  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.22

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 38.10 TO NODE 39.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
 ELEVATION DATA: UPSTREAM(FEET) = 151.20 DOWNSTREAM(FEET) = 150.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.572  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.798  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS A		1.40	0.40	0.200	32	9.57

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF(CFS) = 3.42  
 TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 3.42

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 39.00 TO NODE 39.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.57  
 RAINFALL INTENSITY(INCH/HR) = 2.80  
 AREA-AVERAGED Fm(INCH/HR) = 0.08

AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.20  
 EFFECTIVE STREAM AREA(ACRES) = 1.40  
 TOTAL STREAM AREA(ACRES) = 1.40  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.42

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.53	8.14	3.071	0.40( 0.12)	0.31	2.9	37.10
1	8.62	8.64	2.967	0.40( 0.12)	0.31	3.1	35.10
1	8.62	8.65	2.965	0.40( 0.12)	0.31	3.1	36.10
1	9.22	16.72	2.033	0.40( 0.14)	0.35	5.0	31.00
2	3.42	9.57	2.798	0.40( 0.08)	0.20	1.4	38.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.73	8.14	3.071	0.40( 0.11)	0.28	4.1	37.10
2	11.90	8.64	2.967	0.40( 0.11)	0.28	4.3	35.10
3	11.91	8.65	2.965	0.40( 0.11)	0.28	4.3	36.10
4	12.11	9.57	2.798	0.40( 0.11)	0.28	4.7	38.10
5	11.68	16.72	2.033	0.40( 0.13)	0.32	6.4	31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.11 Tc(MIN.) = 9.57  
 EFFECTIVE AREA(ACRES) = 4.68 AREA-AVERAGED Fm(INCH/HR) = 0.11  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.28  
 TOTAL AREA(ACRES) = 6.4  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 39.00 = 1059.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 39.00 TO NODE 40.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 140.12 DOWNSTREAM(FEET) = 139.79  
 FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.65  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 12.11  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 9.63  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 40.00 = 1085.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.63  
 RAINFALL INTENSITY(INCH/HR) = 2.79  
 AREA-AVERAGED Fm(INCH/HR) = 0.11  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.28  
 EFFECTIVE STREAM AREA(ACRES) = 4.68  
 TOTAL STREAM AREA(ACRES) = 6.40  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.11

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 39.10 TO NODE 40.00 IS CODE = 12

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
 ELEVATION DATA: UPSTREAM(FEET) = 147.50 DOWNSTREAM(FEET) = 144.52

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.979  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.106  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	A	1.01	0.40	0.200	32	7.98

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF(CFS) = 2.75  
 TOTAL AREA(ACRES) = 1.01 PEAK FLOW RATE(CFS) = 2.75

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.98  
 RAINFALL INTENSITY(INCH/HR) = 3.11  
 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.20  
 EFFECTIVE STREAM AREA(ACRES) = 1.01  
 TOTAL STREAM AREA(ACRES) = 1.01  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.75

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.73	8.19	3.059	0.40( 0.11)	0.28	4.1	37.10
1	11.90	8.70	2.956	0.40( 0.11)	0.28	4.3	35.10
1	11.91	8.71	2.954	0.40( 0.11)	0.28	4.3	36.10
1	12.11	9.63	2.789	0.40( 0.11)	0.28	4.7	38.10
1	11.68	16.78	2.029	0.40( 0.13)	0.32	6.4	31.00
2	2.75	7.98	3.106	0.40( 0.08)	0.20	1.0	39.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.36	7.98	3.106	0.40( 0.10)	0.26	5.0	39.10
2	14.44	8.19	3.059	0.40( 0.10)	0.26	5.1	37.10
3	14.52	8.70	2.956	0.40( 0.11)	0.26	5.3	35.10
4	14.52	8.71	2.954	0.40( 0.11)	0.26	5.3	36.10
5	14.58	9.63	2.789	0.40( 0.11)	0.27	5.7	38.10
6	13.45	16.78	2.029	0.40( 0.12)	0.30	7.4	31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.58 Tc(MIN.) = 9.63  
EFFECTIVE AREA(ACRES) = 5.69 AREA-AVERAGED Fm(INCH/HR) = 0.11  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.27  
TOTAL AREA(ACRES) = 7.4  
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 40.00 = 1085.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 40.00 TO NODE 41.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 139.79 DOWNSTREAM(FEET) = 139.10  
FLOW LENGTH(FEET) = 228.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.60  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.58  
PIPE TRAVEL TIME(MIN.) = 0.83 Tc(MIN.) = 10.45  
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 41.00 = 1313.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 41.00 TO NODE 41.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.45  
RAINFALL INTENSITY(INCH/HR) = 2.66  
AREA-AVERAGED Fm(INCH/HR) = 0.11  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.27  
EFFECTIVE STREAM AREA(ACRES) = 5.69  
TOTAL STREAM AREA(ACRES) = 7.41  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 40.10 TO NODE 41.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
ELEVATION DATA: UPSTREAM(FEET) = 148.80 DOWNSTREAM(FEET) = 147.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.826  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.931  
SUBAREA Tc AND LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
APARTMENTS A 2.08 0.40 0.200 32 8.83  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 5.34  
TOTAL AREA(ACRES) = 2.08 PEAK FLOW RATE(CFS) = 5.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 41.00 TO NODE 41.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.83  
RAINFALL INTENSITY(INCH/HR) = 2.93  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 2.08  
TOTAL STREAM AREA(ACRES) = 2.08  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.34

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.36	8.81	2.935	0.40( 0.10)	0.26	5.0	39.10
1	14.44	9.02	2.895	0.40( 0.10)	0.26	5.1	37.10
1	14.52	9.52	2.806	0.40( 0.11)	0.26	5.3	35.10
1	14.52	9.53	2.805	0.40( 0.11)	0.26	5.3	36.10
1	14.58	10.45	2.660	0.40( 0.11)	0.27	5.7	38.10
1	13.45	17.61	1.973	0.40( 0.12)	0.30	7.4	31.00
2	5.34	8.83	2.931	0.40( 0.08)	0.20	2.1	40.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	19.69	8.81	2.935	0.40( 0.10)	0.24	7.1	39.10
2	19.70	8.83	2.931	0.40( 0.10)	0.24	7.1	40.10
3	19.71	9.02	2.895	0.40( 0.10)	0.24	7.2	37.10
4	19.62	9.52	2.806	0.40( 0.10)	0.25	7.4	35.10
5	19.62	9.53	2.805	0.40( 0.10)	0.25	7.4	36.10



6 19.41 10.45 2.660 0.40( 0.10) 0.25 7.8 38.10  
 7 16.99 17.61 1.973 0.40( 0.11) 0.28 9.5 31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.71 Tc(MIN.) = 9.02  
 EFFECTIVE AREA(ACRES) = 7.20 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.24  
 TOTAL AREA(ACRES) = 9.5  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 41.00 = 1313.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.00 TO NODE 42.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 139.10 DOWNSTREAM(FEET) = 139.07  
 FLOW LENGTH(FEET) = 7.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.73  
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 19.71  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 9.04  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 42.00 = 1320.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 42.00 TO NODE 42.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.04  
 RAINFALL INTENSITY(INCH/HR) = 2.89  
 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.24  
 EFFECTIVE STREAM AREA(ACRES) = 7.20  
 TOTAL STREAM AREA(ACRES) = 9.49  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.10 TO NODE 41.20 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 264.00  
 ELEVATION DATA: UPSTREAM(FEET) = 150.70 DOWNSTREAM(FEET) = 150.10

Tc = K\*[ (LENGTH\*\* 3.00)/(ELEVATION CHANGE) ]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.554  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.801  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.63	0.40	0.100	32	9.554

COMMERCIAL A 0.59 0.40 0.100 32 9.55  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 1.47  
 TOTAL AREA(ACRES) = 0.59 PEAK FLOW RATE(CFS) = 1.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.20 TO NODE 41.30 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 145.34  
 FLOW LENGTH(FEET) = 647.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.16  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.47  
 PIPE TRAVEL TIME(MIN.) = 3.41 Tc(MIN.) = 12.97  
 LONGEST FLOWPATH FROM NODE 41.10 TO NODE 41.30 = 911.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.30 TO NODE 41.30 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 12.97  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.351  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.63	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.63 SUBAREA RUNOFF(CFS) = 1.31  
 EFFECTIVE AREA(ACRES) = 1.22 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 2.54

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.30 TO NODE 41.40 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 145.34 DOWNSTREAM(FEET) = 142.67  
 FLOW LENGTH(FEET) = 190.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.32  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.54  
 PIPE TRAVEL TIME(MIN.) = 0.60 Tc(MIN.) = 13.56  
 LONGEST FLOWPATH FROM NODE 41.10 TO NODE 41.40 = 1101.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.40 TO NODE 41.40 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

MAINLINE Tc (MIN.) = 13.56  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.291  
 SUBAREA LOSS RATE DATA (AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL A 0.24 0.40 0.100 32  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.24 SUBAREA RUNOFF (CFS) = 0.49  
 EFFECTIVE AREA (ACRES) = 1.46 AREA-AVERAGED Fm (INCH/HR) = 0.04  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA (ACRES) = 1.5 PEAK FLOW RATE (CFS) = 2.96

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 41.40 TO NODE 42.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====

ELEVATION DATA: UPSTREAM (FEET) = 142.67 DOWNSTREAM (FEET) = 139.07  
 FLOW LENGTH (FEET) = 82.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER (INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.6 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.36  
 ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 2.96  
 PIPE TRAVEL TIME (MIN.) = 0.16 Tc (MIN.) = 13.73  
 LONGEST FLOWPATH FROM NODE 41.10 TO NODE 42.00 = 1183.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 42.00 TO NODE 42.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 13.73  
 RAINFALL INTENSITY (INCH/HR) = 2.28  
 AREA-AVERAGED Fm (INCH/HR) = 0.04  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA (ACRES) = 1.46  
 TOTAL STREAM AREA (ACRES) = 1.46  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 2.96

\*\* CONFLUENCE DATA \*\*  

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	19.69	8.83	2.931	0.40 (0.10)	0.24	7.1	39.10
1	19.70	8.85	2.927	0.40 (0.10)	0.24	7.1	40.10

1	19.71	9.04	2.891	0.40 (0.10)	0.24	7.2	37.10
1	19.62	9.54	2.803	0.40 (0.10)	0.25	7.4	35.10
1	19.62	9.55	2.801	0.40 (0.10)	0.25	7.4	36.10
1	19.41	10.47	2.657	0.40 (0.10)	0.25	7.8	38.10
1	16.99	17.63	1.972	0.40 (0.11)	0.28	9.5	31.00
2	2.96	13.73	2.276	0.40 (0.04)	0.10	1.5	41.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	22.15	8.83	2.931	0.40 (0.09)	0.23	8.0	39.10
2	22.16	8.85	2.927	0.40 (0.09)	0.23	8.0	40.10
3	22.19	9.04	2.891	0.40 (0.09)	0.23	8.2	37.10
4	22.16	9.54	2.803	0.40 (0.09)	0.23	8.4	35.10
5	22.16	9.55	2.801	0.40 (0.09)	0.23	8.4	36.10
6	22.05	10.47	2.657	0.40 (0.09)	0.23	8.9	38.10
7	21.27	13.73	2.276	0.40 (0.10)	0.24	10.0	41.10
8	19.55	17.63	1.972	0.40 (0.10)	0.26	11.0	31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 22.19 Tc (MIN.) = 9.04  
 EFFECTIVE AREA (ACRES) = 8.16 AREA-AVERAGED Fm (INCH/HR) = 0.09  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.23  
 TOTAL AREA (ACRES) = 11.0  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 42.00 = 1320.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====

ELEVATION DATA: UPSTREAM (FEET) = 139.07 DOWNSTREAM (FEET) = 138.55  
 FLOW LENGTH (FEET) = 105.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.5 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 6.21  
 ESTIMATED PIPE DIAMETER (INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 22.19  
 PIPE TRAVEL TIME (MIN.) = 0.28 Tc (MIN.) = 9.32  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 43.00 = 1425.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 43.00 TO NODE 43.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 9.32  
 RAINFALL INTENSITY (INCH/HR) = 2.84  
 AREA-AVERAGED Fm (INCH/HR) = 0.09  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.23

EFFECTIVE STREAM AREA(ACRES) = 8.16  
 TOTAL STREAM AREA(ACRES) = 10.95  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.19

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 42.10 TO NODE 39.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 271.00  
 ELEVATION DATA: UPSTREAM(FEET) = 151.75 DOWNSTREAM(FEET) = 148.70

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.011  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.345  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.27	0.40	0.100	32	7.01

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 0.80  
 TOTAL AREA(ACRES) = 0.27 PEAK FLOW RATE(CFS) = 0.80

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 39.00 TO NODE 43.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 148.70 DOWNSTREAM ELEVATION(FEET) = 146.25  
 STREET LENGTH(FEET) = 356.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 21.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 16.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.23  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.28  
 HALFSTREET FLOOD WIDTH(FEET) = 7.91  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.65  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.47  
 STREET FLOW TRAVEL TIME(MIN.) = 3.60 Tc(MIN.) = 10.61  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.638

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.36	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.36 SUBAREA RUNOFF(CFS) = 0.84  
 EFFECTIVE AREA(ACRES) = 0.63 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.47

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.59  
 FLOW VELOCITY(FEET/SEC.) = 1.72 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.51  
 LONGEST FLOWPATH FROM NODE 42.10 TO NODE 43.00 = 627.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 43.00 TO NODE 43.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.61  
 RAINFALL INTENSITY(INCH/HR) = 2.64  
 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 0.63  
 TOTAL STREAM AREA(ACRES) = 0.63  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.47

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	22.15	9.11	2.879	0.40( 0.09)	0.23	8.0	39.10
1	22.16	9.13	2.875	0.40( 0.09)	0.23	8.0	40.10
1	22.19	9.32	2.841	0.40( 0.09)	0.23	8.2	37.10
1	22.16	9.83	2.757	0.40( 0.09)	0.23	8.4	35.10
1	22.16	9.84	2.755	0.40( 0.09)	0.23	8.4	36.10
1	22.05	10.76	2.617	0.40( 0.09)	0.23	8.9	38.10
1	21.27	14.01	2.249	0.40( 0.10)	0.24	10.0	41.10
1	19.55	17.93	1.953	0.40( 0.10)	0.26	11.0	31.00
2	1.47	10.61	2.638	0.40( 0.04)	0.10	0.6	42.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.53	9.11	2.879	0.40( 0.09)	0.22	8.6	39.10
2	23.55	9.13	2.875	0.40( 0.09)	0.22	8.6	40.10
3	23.59	9.32	2.841	0.40( 0.09)	0.22	8.7	37.10
4	23.59	9.83	2.757	0.40( 0.09)	0.22	9.0	35.10
5	23.59	9.84	2.755	0.40( 0.09)	0.22	9.0	36.10
6	23.54	10.61	2.638	0.40( 0.09)	0.22	9.4	42.10
7	23.51	10.76	2.617	0.40( 0.09)	0.22	9.5	38.10
8	22.52	14.01	2.249	0.40( 0.09)	0.23	10.6	41.10

9 20.63 17.93 1.953 0.40( 0.10) 0.25 11.6 31.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 23.59 Tc(MIN.) = 9.83
EFFECTIVE AREA(ACRES) = 9.01 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.22
TOTAL AREA(ACRES) = 11.6
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 43.00 = 1425.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 43.00 TO NODE 44.00 IS CODE = 31
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 138.55 DOWNSTREAM(FEET) = 138.35
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.30
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.59
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 9.93
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 44.00 = 1465.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 44.00 TO NODE 44.00 IS CODE = 1
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.93
RAINFALL INTENSITY(INCH/HR) = 2.74
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.22
EFFECTIVE STREAM AREA(ACRES) = 9.01
TOTAL STREAM AREA(ACRES) = 11.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.59

\*\*\*\*\*
FLOW PROCESS FROM NODE 43.10 TO NODE 40.00 IS CODE = 21
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 265.00
ELEVATION DATA: UPSTREAM(FEET) = 150.73 DOWNSTREAM(FEET) = 148.33

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.257
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.279
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 0.22 0.40 0.100 32 7.26

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 0.64
TOTAL AREA(ACRES) = 0.22 PEAK FLOW RATE(CFS) = 0.64

\*\*\*\*\*
FLOW PROCESS FROM NODE 40.00 TO NODE 44.00 IS CODE = 61
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 148.33 DOWNSTREAM ELEVATION(FEET) = 146.08
STREET LENGTH(FEET) = 364.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 21.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 16.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.98
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.27
HALFSSTREET FLOOD WIDTH(FEET) = 7.28
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.51
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.41
STREET FLOW TRAVEL TIME(MIN.) = 4.01 Tc(MIN.) = 11.27
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.549

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.30 0.40 0.100 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 0.68
EFFECTIVE AREA(ACRES) = 0.52 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 1.17

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.28 HALFSSTREET FLOOD WIDTH(FEET) = 7.91
FLOW VELOCITY(FEET/SEC.) = 1.58 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.45
LONGEST FLOWPATH FROM NODE 43.10 TO NODE 44.00 = 629.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 44.00 TO NODE 44.00 IS CODE = 81
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 11.27
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.549
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 APARTMENTS A 1.46 0.40 0.200 32  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA AREA (ACRES) = 1.46 SUBAREA RUNOFF (CFS) = 3.24  
 EFFECTIVE AREA (ACRES) = 1.98 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.17  
 TOTAL AREA (ACRES) = 2.0 PEAK FLOW RATE (CFS) = 4.42

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 44.00 TO NODE 44.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 11.27  
 RAINFALL INTENSITY (INCH/HR) = 2.55  
 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.17  
 EFFECTIVE STREAM AREA (ACRES) = 1.98  
 TOTAL STREAM AREA (ACRES) = 1.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.42

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.53	9.21	2.860	0.40( 0.09)	0.22	8.6	39.10
1	23.55	9.23	2.856	0.40( 0.09)	0.22	8.6	40.10
1	23.59	9.43	2.823	0.40( 0.09)	0.22	8.7	37.10
1	23.59	9.93	2.740	0.40( 0.09)	0.22	9.0	35.10
1	23.59	9.94	2.738	0.40( 0.09)	0.22	9.0	36.10
1	23.54	10.71	2.623	0.40( 0.09)	0.22	9.4	42.10
1	23.51	10.86	2.603	0.40( 0.09)	0.22	9.5	38.10
1	22.52	14.12	2.239	0.40( 0.09)	0.23	10.6	41.10
1	20.63	18.04	1.946	0.40( 0.10)	0.25	11.6	31.00
2	4.42	11.27	2.549	0.40( 0.07)	0.17	2.0	43.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	27.60	9.21	2.860	0.40( 0.08)	0.21	10.2	39.10
2	27.62	9.23	2.856	0.40( 0.08)	0.21	10.2	40.10
3	27.69	9.43	2.823	0.40( 0.08)	0.21	10.4	37.10
4	27.79	9.93	2.740	0.40( 0.09)	0.21	10.8	35.10
5	27.79	9.94	2.738	0.40( 0.09)	0.21	10.8	36.10
6	27.87	10.71	2.623	0.40( 0.09)	0.21	11.3	42.10
7	27.86	10.86	2.603	0.40( 0.09)	0.21	11.4	38.10
8	27.81	11.27	2.549	0.40( 0.09)	0.21	11.6	43.10
9	26.39	14.12	2.239	0.40( 0.09)	0.22	12.6	41.10

10 23.98 18.04 1.946 0.40( 0.09) 0.24 13.6 31.00  
 COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 27.87 Tc (MIN.) = 10.71  
 EFFECTIVE AREA (ACRES) = 11.33 AREA-AVERAGED Fm (INCH/HR) = 0.09  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.21  
 TOTAL AREA (ACRES) = 13.6  
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 44.00 = 1465.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 61.00 TO NODE 62.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
 =====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
 ELEVATION DATA: UPSTREAM (FEET) = 155.00 DOWNSTREAM (FEET) = 152.70

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 8.404  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.015  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 APARTMENTS A 1.26 0.40 0.200 32 8.40  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF (CFS) = 3.33  
 TOTAL AREA (ACRES) = 1.26 PEAK FLOW RATE (CFS) = 3.33

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 62.00 TO NODE 63.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<  
 =====

UPSTREAM ELEVATION (FEET) = 152.70 DOWNSTREAM ELEVATION (FEET) = 151.40  
 STREET LENGTH (FEET) = 210.00 CURB HEIGHT (INCHES) = 6.0  
 STREET HALFWIDTH (FEET) = 21.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 16.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 5.83  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.44  
 HALFSTREET FLOOD WIDTH (FEET) = 15.59  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 2.29  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 1.00  
 STREET FLOW TRAVEL TIME (MIN.) = 1.53 Tc (MIN.) = 9.93

```

* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.739
SUBAREA LOSS RATE DATA (AMC II):
  DEVELOPMENT TYPE/      SCS SOIL  AREA   Fp      Ap      SCS
  LAND USE              GROUP (ACRES) (INCH/HR) (DECIMAL) CN
APARTMENTS              A      2.09   0.40   0.200   32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA (ACRES) = 2.09   SUBAREA RUNOFF (CFS) = 5.00
EFFECTIVE AREA (ACRES) = 3.35   AREA-AVERAGED Fm (INCH/HR) = 0.08
AREA-AVERAGED Fp (INCH/HR) = 0.40   AREA-AVERAGED Ap = 0.20
TOTAL AREA (ACRES) = 3.3   PEAK FLOW RATE (CFS) = 8.02

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH (FEET) = 0.48   HALFSTREET FLOOD WIDTH (FEET) = 17.72
FLOW VELOCITY (FEET/SEC.) = 2.46   DEPTH*VELOCITY (FT*FT/SEC.) = 1.18
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 63.00 = 510.00 FEET.

*****
FLOW PROCESS FROM NODE 63.00 TO NODE 63.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION (MIN.) = 9.93
RAINFALL INTENSITY (INCH/HR) = 2.74
AREA-AVERAGED Fm (INCH/HR) = 0.08
AREA-AVERAGED Fp (INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA (ACRES) = 3.35
TOTAL STREAM AREA (ACRES) = 3.35
PEAK FLOW RATE (CFS) AT CONFLUENCE = 8.02

*****
FLOW PROCESS FROM NODE 62.10 TO NODE 63.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
-----
INITIAL SUBAREA FLOW-LENGTH (FEET) = 246.00
ELEVATION DATA: UPSTREAM (FEET) = 153.90   DOWNSTREAM (FEET) = 151.41

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)] ** 0.20
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.343
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.257
SUBAREA Tc AND LOSS RATE DATA (AMC II):
  DEVELOPMENT TYPE/      SCS SOIL  AREA   Fp      Ap      SCS   Tc
  LAND USE              GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
APARTMENTS              A      1.35   0.40   0.200   32   7.34
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF (CFS) = 3.86
TOTAL AREA (ACRES) = 1.35   PEAK FLOW RATE (CFS) = 3.86

*****
FLOW PROCESS FROM NODE 63.00 TO NODE 63.00 IS CODE = 1

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-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
-----
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION (MIN.) = 7.34
RAINFALL INTENSITY (INCH/HR) = 3.26
AREA-AVERAGED Fm (INCH/HR) = 0.08
AREA-AVERAGED Fp (INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA (ACRES) = 1.35
TOTAL STREAM AREA (ACRES) = 1.35
PEAK FLOW RATE (CFS) AT CONFLUENCE = 3.86

** CONFLUENCE DATA **
STREAM   Q      Tc   Intensity   Fp(Fm)   Ap      Ae      HEADWATER
NUMBER  (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1        8.02  9.93  3.257  0.40( 0.08) 0.20   3.3   61.00
2        3.86  7.34  3.257  0.40( 0.08) 0.20   1.4   62.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM   Q      Tc   Intensity   Fp(Fm)   Ap      Ae      HEADWATER
NUMBER  (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1       10.94  7.34  3.257  0.40( 0.08) 0.20   3.8   62.10
2       11.25  9.93  2.739  0.40( 0.08) 0.20   4.7   61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE (CFS) = 11.25   Tc (MIN.) = 9.93
EFFECTIVE AREA (ACRES) = 4.70   AREA-AVERAGED Fm (INCH/HR) = 0.08
AREA-AVERAGED Fp (INCH/HR) = 0.40   AREA-AVERAGED Ap = 0.20
TOTAL AREA (ACRES) = 4.7
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 63.00 = 510.00 FEET.

*****
FLOW PROCESS FROM NODE 63.00 TO NODE 64.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
-----
ELEVATION DATA: UPSTREAM (FEET) = 147.30   DOWNSTREAM (FEET) = 146.70
FLOW LENGTH (FEET) = 305.00   MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 3.69
ESTIMATED PIPE DIAMETER (INCH) = 27.00   NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 11.25
PIPE TRAVEL TIME (MIN.) = 1.38   Tc (MIN.) = 11.31
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 64.00 = 815.00 FEET.

*****
FLOW PROCESS FROM NODE 64.00 TO NODE 64.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.31
RAINFALL INTENSITY(INCH/HR) = 2.54
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 4.70
TOTAL STREAM AREA(ACRES) = 4.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.25

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*****
FLOW PROCESS FROM NODE 63.10 TO NODE 64.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
-----

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```

INITIAL SUBAREA FLOW-LENGTH( FEET) = 130.00
ELEVATION DATA: UPSTREAM( FEET) = 152.17 DOWNSTREAM( FEET) = 151.43

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.990
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.660
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 0.15 0.40 0.100 32 5.99
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 0.49
TOTAL AREA(ACRES) = 0.15 PEAK FLOW RATE(CFS) = 0.49

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*****
FLOW PROCESS FROM NODE 64.00 TO NODE 64.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
-----

```

```

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.99
RAINFALL INTENSITY(INCH/HR) = 3.66
AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 0.15
TOTAL STREAM AREA(ACRES) = 0.15
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.49

```

```

** CONFLUENCE DATA **

```

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.94	8.73	2.950	0.40( 0.08)	0.20	3.8	62.10
1	11.25	11.31	2.543	0.40( 0.08)	0.20	4.7	61.00
2	0.49	5.99	3.660	0.40( 0.04)	0.10	0.2	63.10

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

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** PEAK FLOW RATE TABLE **

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STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.86	5.99	3.660	0.40( 0.08)	0.19	2.8	63.10
2	11.33	8.73	2.950	0.40( 0.08)	0.20	4.0	62.10
3	11.59	11.31	2.543	0.40( 0.08)	0.20	4.8	61.00

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 11.59 Tc(MIN.) = 11.31
EFFECTIVE AREA(ACRES) = 4.85 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 4.8
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 64.00 = 815.00 FEET.

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```

*****
FLOW PROCESS FROM NODE 64.00 TO NODE 65.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
-----

```

```

ELEVATION DATA: UPSTREAM( FEET) = 146.70 DOWNSTREAM( FEET) = 146.65
FLOW LENGTH( FEET) = 17.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.6 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 4.22
ESTIMATED PIPE DIAMETER( INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.59
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 11.38
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 65.00 = 832.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 65.00 TO NODE 65.00 IS CODE = 1
-----

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```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
-----

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```

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.38
RAINFALL INTENSITY(INCH/HR) = 2.53
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 4.85
TOTAL STREAM AREA(ACRES) = 4.85
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.59

```

```

*****
FLOW PROCESS FROM NODE 64.10 TO NODE 65.00 IS CODE = 21
-----

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
-----

```

```

INITIAL SUBAREA FLOW-LENGTH( FEET) = 279.00

```

ELEVATION DATA: UPSTREAM(FEET) = 153.50 DOWNSTREAM(FEET) = 151.43

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.217

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.054

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	A	0.78	0.40	0.200	32	8.22

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 2.09  
TOTAL AREA(ACRES) = 0.78 PEAK FLOW RATE(CFS) = 2.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 65.00 TO NODE 65.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.22  
RAINFALL INTENSITY(INCH/HR) = 3.05  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 0.78  
TOTAL STREAM AREA(ACRES) = 0.78  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.09

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.86	6.06	3.637	0.40( 0.08)	0.19	2.8	63.10
1	11.33	8.79	2.937	0.40( 0.08)	0.20	4.0	62.10
1	11.59	11.38	2.534	0.40( 0.08)	0.20	4.8	61.00
2	2.09	8.22	3.054	0.40( 0.08)	0.20	0.8	64.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.70	6.06	3.637	0.40( 0.08)	0.20	3.4	63.10
2	13.11	8.22	3.054	0.40( 0.08)	0.20	4.5	64.10
3	13.34	8.79	2.937	0.40( 0.08)	0.20	4.8	62.10
4	13.31	11.38	2.534	0.40( 0.08)	0.20	5.6	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.34 Tc(MIN.) = 8.79  
EFFECTIVE AREA(ACRES) = 4.76 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 5.6  
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 65.00 = 832.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 65.00 TO NODE 66.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 146.65 DOWNSTREAM(FEET) = 146.36  
FLOW LENGTH(FEET) = 89.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.68  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 13.34  
PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 9.11  
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 66.00 = 921.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.11  
RAINFALL INTENSITY(INCH/HR) = 2.88  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.20  
EFFECTIVE STREAM AREA(ACRES) = 4.76  
TOTAL STREAM AREA(ACRES) = 5.63  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 65.10 TO NODE 66.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 163.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.16 DOWNSTREAM(FEET) = 151.82

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.449

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.864

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.16	0.40	0.100	32	5.45

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA RUNOFF(CFS) = 0.55  
TOTAL AREA(ACRES) = 0.16 PEAK FLOW RATE(CFS) = 0.55

\*\*\*\*\*  
FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 1



>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.45  
 RAINFALL INTENSITY(INCH/HR) = 3.86  
 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 0.16  
 TOTAL STREAM AREA(ACRES) = 0.16  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.55

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.70	6.39	3.527	0.40( 0.08)	0.20	3.4	63.10
1	13.11	8.53	2.988	0.40( 0.08)	0.20	4.5	64.10
1	13.34	9.11	2.878	0.40( 0.08)	0.20	4.8	62.10
1	13.31	11.70	2.495	0.40( 0.08)	0.20	5.6	61.00
2	0.55	5.45	3.864	0.40( 0.04)	0.10	0.2	65.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.50	5.45	3.864	0.40( 0.08)	0.19	3.0	65.10
2	12.20	6.39	3.527	0.40( 0.08)	0.19	3.5	63.10
3	13.53	8.53	2.988	0.40( 0.08)	0.19	4.7	64.10
4	13.75	9.11	2.878	0.40( 0.08)	0.19	4.9	62.10
5	13.66	11.70	2.495	0.40( 0.08)	0.19	5.8	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 13.75 Tc(MIN.) = 9.11  
 EFFECTIVE AREA(ACRES) = 4.92 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
 TOTAL AREA(ACRES) = 5.8  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 66.00 = 921.00 FEET.

=====

FLOW PROCESS FROM NODE 66.00 TO NODE 67.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 146.36 DOWNSTREAM(FEET) = 146.32  
 FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.12  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 13.75  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 9.14  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 67.00 = 931.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 67.00 TO NODE 67.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.14  
 RAINFALL INTENSITY(INCH/HR) = 2.87  
 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.19  
 EFFECTIVE STREAM AREA(ACRES) = 4.92  
 TOTAL STREAM AREA(ACRES) = 5.79  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.10 TO NODE 67.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
 ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 151.92

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.574  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.980  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	A	0.90	0.40	0.200	32	8.57

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF(CFS) = 2.35  
 TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 67.00 TO NODE 67.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.57  
 RAINFALL INTENSITY(INCH/HR) = 2.98  
 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.20  
 EFFECTIVE STREAM AREA(ACRES) = 0.90  
 TOTAL STREAM AREA(ACRES) = 0.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.35

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.50	5.48	3.850	0.40( 0.08)	0.19	3.0	65.10
1	12.20	6.43	3.516	0.40( 0.08)	0.19	3.5	63.10
1	13.53	8.57	2.981	0.40( 0.08)	0.19	4.7	64.10
1	13.75	9.14	2.872	0.40( 0.08)	0.19	4.9	62.10
1	13.66	11.73	2.491	0.40( 0.08)	0.19	5.8	61.00
2	2.35	8.57	2.980	0.40( 0.08)	0.20	0.9	66.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.45	5.48	3.850	0.40( 0.08)	0.19	3.6	65.10
2	14.28	6.43	3.516	0.40( 0.08)	0.19	4.2	63.10
3	15.88	8.57	2.981	0.40( 0.08)	0.19	5.6	64.10
4	15.89	8.57	2.980	0.40( 0.08)	0.19	5.6	66.10
5	16.01	9.14	2.872	0.40( 0.08)	0.19	5.8	62.10
6	15.62	11.73	2.491	0.40( 0.08)	0.20	6.7	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.01 Tc(MIN.) = 9.14  
EFFECTIVE AREA(ACRES) = 5.82 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
TOTAL AREA(ACRES) = 6.7  
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 67.00 = 931.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 67.00 TO NODE 68.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 146.32 DOWNSTREAM(FEET) = 144.80  
FLOW LENGTH(FEET) = 463.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 21.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.82  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.01  
PIPE TRAVEL TIME(MIN.) = 1.60 Tc(MIN.) = 10.75  
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 68.00 = 1394.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 68.00 TO NODE 68.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.75  
RAINFALL INTENSITY(INCH/HR) = 2.62  
AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.19

EFFECTIVE STREAM AREA(ACRES) = 5.82  
TOTAL STREAM AREA(ACRES) = 6.69  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.01

\*\*\*\*\*  
FLOW PROCESS FROM NODE 67.10 TO NODE 68.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
ELEVATION DATA: UPSTREAM(FEET) = 154.16 DOWNSTREAM(FEET) = 150.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.185  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.298  
SUBAREA Tc AND LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCSSOIL AREA Fp Ap SCSS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
COMMERCIAL A 0.27 0.40 0.100 32 7.19  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA RUNOFF(CFS) = 0.79  
TOTAL AREA(ACRES) = 0.27 PEAK FLOW RATE(CFS) = 0.79

\*\*\*\*\*  
FLOW PROCESS FROM NODE 68.00 TO NODE 68.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.19  
RAINFALL INTENSITY(INCH/HR) = 3.30  
AREA-AVERAGED Fm(INCH/HR) = 0.04  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 0.10  
EFFECTIVE STREAM AREA(ACRES) = 0.27  
TOTAL STREAM AREA(ACRES) = 0.27  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.79

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.45	7.12	3.314	0.40( 0.08)	0.19	3.6	65.10
1	14.28	8.05	3.090	0.40( 0.08)	0.19	4.2	63.10
1	15.88	10.17	2.702	0.40( 0.08)	0.19	5.6	64.10
1	15.89	10.18	2.702	0.40( 0.08)	0.19	5.6	66.10
1	16.01	10.75	2.619	0.40( 0.08)	0.19	5.8	62.10
1	15.62	13.33	2.314	0.40( 0.08)	0.20	6.7	61.00
2	0.79	7.19	3.298	0.40( 0.04)	0.10	0.3	67.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.24	7.12	3.314	0.40( 0.07)	0.19	3.9	65.10
2	14.30	7.19	3.298	0.40( 0.07)	0.19	3.9	67.10
3	15.03	8.05	3.090	0.40( 0.07)	0.19	4.5	63.10
4	16.53	10.17	2.702	0.40( 0.08)	0.19	5.8	64.10
5	16.53	10.18	2.702	0.40( 0.08)	0.19	5.8	66.10
6	16.64	10.75	2.619	0.40( 0.08)	0.19	6.1	62.10
7	16.17	13.33	2.314	0.40( 0.08)	0.19	7.0	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.64 Tc(MIN.) = 10.75  
 EFFECTIVE AREA(ACRES) = 6.09 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
 TOTAL AREA(ACRES) = 7.0  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 68.00 = 1394.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 68.00 TO NODE 69.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 144.80 DOWNSTREAM(FEET) = 143.71  
 FLOW LENGTH(FEET) = 118.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.31  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 16.64  
 PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 11.02  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 69.00 = 1512.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 69.00 TO NODE 69.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.02  
 RAINFALL INTENSITY(INCH/HR) = 2.58  
 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.19  
 EFFECTIVE STREAM AREA(ACRES) = 6.09  
 TOTAL STREAM AREA(ACRES) = 6.96  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.64

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 68.10 TO NODE 68.20 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 265.00

ELEVATION DATA: UPSTREAM(FEET) = 154.10 DOWNSTREAM(FEET) = 151.14

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.959  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.359  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.20	0.40	0.100	32	6.96

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 0.60  
 TOTAL AREA(ACRES) = 0.20 PEAK FLOW RATE(CFS) = 0.60

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 68.20 TO NODE 69.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 151.14 DOWNSTREAM ELEVATION(FEET) = 148.80  
 STREET LENGTH(FEET) = 185.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 21.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 16.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.80  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.23  
 HALFSTREET FLOOD WIDTH(FEET) = 5.41  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.94  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.45  
 STREET FLOW TRAVEL TIME(MIN.) = 1.59 Tc(MIN.) = 8.55  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.985

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.15	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.15 SUBAREA RUNOFF(CFS) = 0.40  
 EFFECTIVE AREA(ACRES) = 0.35 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 0.93

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.91  
 FLOW VELOCITY(FEET/SEC.) = 1.99 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.49  
 LONGEST FLOWPATH FROM NODE 68.10 TO NODE 69.00 = 450.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 69.00 TO NODE 69.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====

MAINLINE Tc (MIN.) = 8.55  
 \* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.985  
 SUBAREA LOSS RATE DATA (AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 APARTMENTS A 1.99 0.40 0.200 32  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA AREA (ACRES) = 1.99 SUBAREA RUNOFF (CFS) = 5.20  
 EFFECTIVE AREA (ACRES) = 2.34 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
 TOTAL AREA (ACRES) = 2.3 PEAK FLOW RATE (CFS) = 6.13

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 69.00 TO NODE 69.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 8.55  
 RAINFALL INTENSITY (INCH/HR) = 2.99  
 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.19  
 EFFECTIVE STREAM AREA (ACRES) = 2.34  
 TOTAL STREAM AREA (ACRES) = 2.34  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 6.13

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.24	7.41	3.240	0.40 ( 0.07)	0.19	3.9	65.10
1	14.30	7.47	3.225	0.40 ( 0.07)	0.19	3.9	67.10
1	15.03	8.32	3.031	0.40 ( 0.07)	0.19	4.5	63.10
1	16.53	10.44	2.662	0.40 ( 0.08)	0.19	5.8	64.10
1	16.53	10.45	2.661	0.40 ( 0.08)	0.19	5.8	66.10
1	16.64	11.02	2.582	0.40 ( 0.08)	0.19	6.1	62.10
1	16.17	13.60	2.288	0.40 ( 0.08)	0.19	7.0	61.00
2	6.13	8.55	2.985	0.40 ( 0.07)	0.19	2.3	68.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.02	7.41	3.240	0.40 ( 0.07)	0.19	5.9	65.10
2	20.10	7.47	3.225	0.40 ( 0.07)	0.19	5.9	67.10

3	21.09	8.32	3.031	0.40 ( 0.07)	0.19	6.7	63.10
4	21.32	8.55	2.985	0.40 ( 0.07)	0.19	6.9	68.10
5	21.98	10.44	2.662	0.40 ( 0.08)	0.19	8.2	64.10
6	21.98	10.45	2.661	0.40 ( 0.08)	0.19	8.2	66.10
7	21.92	11.02	2.582	0.40 ( 0.08)	0.19	8.4	62.10
8	20.83	13.60	2.288	0.40 ( 0.08)	0.19	9.3	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 21.98 Tc (MIN.) = 10.45  
 EFFECTIVE AREA (ACRES) = 8.18 AREA-AVERAGED Fm (INCH/HR) = 0.08  
 AREA-AVERAGED Fp (INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19  
 TOTAL AREA (ACRES) = 9.3  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 69.00 = 1512.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 69.00 TO NODE 70.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM (FEET) = 143.71 DOWNSTREAM (FEET) = 142.45  
 FLOW LENGTH (FEET) = 180.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.9 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 6.99  
 ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 21.98  
 PIPE TRAVEL TIME (MIN.) = 0.43 Tc (MIN.) = 10.88  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 70.00 = 1692.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 70.00 TO NODE 70.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 10.88  
 RAINFALL INTENSITY (INCH/HR) = 2.60  
 AREA-AVERAGED Fm (INCH/HR) = 0.08  
 AREA-AVERAGED Fp (INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.19  
 EFFECTIVE STREAM AREA (ACRES) = 8.18  
 TOTAL STREAM AREA (ACRES) = 9.30  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 21.98

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 68.00 TO NODE 70.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
 =====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00  
 ELEVATION DATA: UPSTREAM (FEET) = 150.40 DOWNSTREAM (FEET) = 146.65  
 Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.151

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.307  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL A 0.36 0.40 0.100 32 7.15  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 1.06  
 TOTAL AREA(ACRES) = 0.36 PEAK FLOW RATE(CFS) = 1.06

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 70.00 TO NODE 70.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

-----  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.15  
 RAINFALL INTENSITY(INCH/HR) = 3.31  
 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 0.36  
 TOTAL STREAM AREA(ACRES) = 0.36  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.06

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.02	7.85	3.136	0.40( 0.07)	0.19	5.9	65.10
1	20.10	7.91	3.122	0.40( 0.07)	0.19	5.9	67.10
1	21.09	8.76	2.945	0.40( 0.07)	0.19	6.7	63.10
1	21.32	8.98	2.902	0.40( 0.07)	0.19	6.9	68.10
1	21.98	10.87	2.602	0.40( 0.08)	0.19	8.2	64.10
1	21.98	10.88	2.601	0.40( 0.08)	0.19	8.2	66.10
1	21.92	11.44	2.526	0.40( 0.08)	0.19	8.4	62.10
1	20.83	14.04	2.247	0.40( 0.08)	0.19	9.3	61.00
2	1.06	7.15	3.307	0.40( 0.04)	0.10	0.4	68.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.32	7.15	3.307	0.40( 0.07)	0.18	5.7	68.00
2	21.02	7.85	3.136	0.40( 0.07)	0.18	6.2	65.10
3	21.10	7.91	3.122	0.40( 0.07)	0.18	6.3	67.10
4	22.03	8.76	2.945	0.40( 0.07)	0.18	7.1	63.10
5	22.24	8.98	2.902	0.40( 0.07)	0.18	7.3	68.10
6	22.81	10.87	2.602	0.40( 0.07)	0.18	8.5	64.10
7	22.81	10.88	2.601	0.40( 0.07)	0.18	8.5	66.10
8	22.72	11.44	2.526	0.40( 0.07)	0.19	8.8	62.10
9	21.54	14.04	2.247	0.40( 0.07)	0.19	9.7	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 22.81 Tc(MIN.) = 10.88  
 EFFECTIVE AREA(ACRES) = 8.54 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.18  
 TOTAL AREA(ACRES) = 9.7  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 70.00 = 1692.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 70.00 TO NODE 71.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

-----  
 ELEVATION DATA: UPSTREAM(FEET) = 142.45 DOWNSTREAM(FEET) = 142.36  
 FLOW LENGTH(FEET) = 12.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.24  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 22.81  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 10.90  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 71.00 = 1704.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 71.00 TO NODE 71.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

-----  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.90  
 RAINFALL INTENSITY(INCH/HR) = 2.60  
 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.18  
 EFFECTIVE STREAM AREA(ACRES) = 8.54  
 TOTAL STREAM AREA(ACRES) = 9.66  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.81

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 70.10 TO NODE 71.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

-----  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 232.00  
 ELEVATION DATA: UPSTREAM(FEET) = 149.50 DOWNSTREAM(FEET) = 146.60

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.452  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.508  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL A 0.77 0.40 0.100 32 6.45  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA RUNOFF(CFS) = 2.40  
 TOTAL AREA(ACRES) = 0.77 PEAK FLOW RATE(CFS) = 2.40

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 71.00 TO NODE 71.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.45  
 RAINFALL INTENSITY(INCH/HR) = 3.51  
 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 0.77  
 TOTAL STREAM AREA(ACRES) = 0.77  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.40

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.32	7.18	3.300	0.40( 0.07)	0.18	5.7	68.00
1	21.02	7.87	3.129	0.40( 0.07)	0.18	6.2	65.10
1	21.10	7.94	3.115	0.40( 0.07)	0.18	6.3	67.10
1	22.03	8.78	2.939	0.40( 0.07)	0.18	7.1	63.10
1	22.24	9.01	2.897	0.40( 0.07)	0.18	7.3	68.10
1	22.81	10.90	2.598	0.40( 0.07)	0.18	8.5	64.10
1	22.81	10.90	2.597	0.40( 0.07)	0.18	8.5	66.10
1	22.72	11.47	2.522	0.40( 0.07)	0.19	8.8	62.10
1	21.54	14.06	2.244	0.40( 0.07)	0.19	9.7	61.00
2	2.40	6.45	3.508	0.40( 0.04)	0.10	0.8	70.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	21.85	6.45	3.508	0.40( 0.07)	0.17	5.9	70.10
2	22.58	7.18	3.300	0.40( 0.07)	0.17	6.5	68.00
3	23.16	7.87	3.129	0.40( 0.07)	0.17	7.0	65.10
4	23.23	7.94	3.115	0.40( 0.07)	0.17	7.1	67.10
5	24.04	8.78	2.939	0.40( 0.07)	0.17	7.9	63.10
6	24.22	9.01	2.897	0.40( 0.07)	0.17	8.1	68.10
7	24.58	10.90	2.598	0.40( 0.07)	0.18	9.3	64.10
8	24.58	10.90	2.597	0.40( 0.07)	0.18	9.3	66.10
9	24.44	11.47	2.522	0.40( 0.07)	0.18	9.6	62.10
10	23.07	14.06	2.244	0.40( 0.07)	0.18	10.4	61.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 24.58 Tc(MIN.) = 10.90  
 EFFECTIVE AREA(ACRES) = 9.30 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.18  
 TOTAL AREA(ACRES) = 10.4

LONGEST FLOWPATH FROM NODE 61.00 TO NODE 71.00 = 1704.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 71.00 TO NODE 72.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 142.36 DOWNSTREAM(FEET) = 141.50  
 FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.69  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 24.58  
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.99  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 72.00 = 1759.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 72.00 TO NODE 72.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.99  
 RAINFALL INTENSITY(INCH/HR) = 2.58  
 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.18  
 EFFECTIVE STREAM AREA(ACRES) = 9.30  
 TOTAL STREAM AREA(ACRES) = 10.43  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.58

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 71.10 TO NODE 71.20 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 275.00  
 ELEVATION DATA: UPSTREAM(FEET) = 150.10 DOWNSTREAM(FEET) = 149.80

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.247  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.551  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.89	0.40	0.100	32	11.25

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 2.01  
 TOTAL AREA(ACRES) = 0.89 PEAK FLOW RATE(CFS) = 2.01

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 71.20 TO NODE 71.30 IS CODE = 51

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-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 149.80 DOWNSTREAM( FEET) = 147.60
CHANNEL LENGTH THRU SUBAREA( FEET) = 993.00 CHANNEL SLOPE = 0.0022
CHANNEL BASE( FEET) = 10.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH( FEET) = 1.00
* 10 YEAR RAINFALL INTENSITY( INCH/HR) = 1.810
SUBAREA LOSS RATE DATA( AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 6.14 0.40 0.100 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp( INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS) = 7.02
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 1.80
AVERAGE FLOW DEPTH( FEET) = 0.30 TRAVEL TIME( MIN.) = 9.22
Tc( MIN.) = 20.46
SUBAREA AREA( ACRES) = 6.14 SUBAREA RUNOFF( CFS) = 9.78
EFFECTIVE AREA( ACRES) = 7.03 AREA-AVERAGED Fm( INCH/HR) = 0.04
AREA-AVERAGED Fp( INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.10
TOTAL AREA( ACRES) = 7.0 PEAK FLOW RATE( CFS) = 11.20

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END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) = 0.39 FLOW VELOCITY( FEET/SEC.) = 2.09
LONGEST FLOWPATH FROM NODE 71.10 TO NODE 71.30 = 1268.00 FEET.

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*****
FLOW PROCESS FROM NODE 71.30 TO NODE 72.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 147.60 DOWNSTREAM( FEET) = 141.50
FLOW LENGTH( FEET) = 97.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER( INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 13.76
ESTIMATED PIPE DIAMETER( INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 11.20
PIPE TRAVEL TIME( MIN.) = 0.12 Tc( MIN.) = 20.58
LONGEST FLOWPATH FROM NODE 71.10 TO NODE 72.00 = 1365.00 FEET.

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*****
FLOW PROCESS FROM NODE 72.00 TO NODE 72.00 IS CODE = 1
-----

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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION( MIN.) = 20.58
RAINFALL INTENSITY( INCH/HR) = 1.80
AREA-AVERAGED Fm( INCH/HR) = 0.04
AREA-AVERAGED Fp( INCH/HR) = 0.40

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AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA( ACRES) = 7.03
TOTAL STREAM AREA( ACRES) = 7.03
PEAK FLOW RATE( CFS) AT CONFLUENCE = 11.20

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	21.85	6.55	3.478	0.40( 0.07)	0.17	5.9	70.10
1	22.58	7.27	3.275	0.40( 0.07)	0.17	6.5	68.00
1	23.16	7.97	3.108	0.40( 0.07)	0.17	7.0	65.10
1	23.23	8.03	3.094	0.40( 0.07)	0.17	7.1	67.10
1	24.04	8.88	2.921	0.40( 0.07)	0.17	7.9	63.10
1	24.22	9.10	2.880	0.40( 0.07)	0.17	8.1	68.10
1	24.58	10.99	2.585	0.40( 0.07)	0.18	9.3	64.10
1	24.58	11.00	2.584	0.40( 0.07)	0.18	9.3	66.10
1	24.44	11.57	2.511	0.40( 0.07)	0.18	9.6	62.10
1	23.07	14.16	2.236	0.40( 0.07)	0.18	10.4	61.00
2	11.20	20.58	1.805	0.40( 0.04)	0.10	7.0	71.10

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

```

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	28.79	6.55	3.478	0.40( 0.06)	0.15	8.2	70.10
2	29.84	7.27	3.275	0.40( 0.06)	0.15	9.0	68.00
3	30.71	7.97	3.108	0.40( 0.06)	0.15	9.7	65.10
4	30.79	8.03	3.094	0.40( 0.06)	0.15	9.8	67.10
5	31.93	8.88	2.921	0.40( 0.06)	0.15	10.9	63.10
6	32.20	9.10	2.880	0.40( 0.06)	0.15	11.2	68.10
7	33.21	10.99	2.585	0.40( 0.06)	0.16	13.1	64.10
8	33.21	11.00	2.584	0.40( 0.06)	0.16	13.1	66.10
9	33.26	11.57	2.511	0.40( 0.06)	0.16	13.5	62.10
10	32.66	14.16	2.236	0.40( 0.06)	0.15	15.3	61.00
11	29.68	20.58	1.805	0.40( 0.06)	0.15	17.5	71.10

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE( CFS) = 33.26 Tc( MIN.) = 11.57
EFFECTIVE AREA( ACRES) = 13.51 AREA-AVERAGED Fm( INCH/HR) = 0.06
AREA-AVERAGED Fp( INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.16
TOTAL AREA( ACRES) = 17.5
LONGEST FLOWPATH FROM NODE 61.00 TO NODE 72.00 = 1759.00 FEET.

```

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*****
FLOW PROCESS FROM NODE 72.00 TO NODE 73.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 141.50 DOWNSTREAM( FEET) = 140.82
FLOW LENGTH( FEET) = 287.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 28.2 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 5.18
ESTIMATED PIPE DIAMETER( INCH) = 39.00 NUMBER OF PIPES = 1

```

PIPE-FLOW(CFS) = 33.26  
 PIPE TRAVEL TIME(MIN.) = 0.92 Tc(MIN.) = 12.49  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 73.00 = 2046.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 73.00 TO NODE 73.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.49  
 RAINFALL INTENSITY(INCH/HR) = 2.40  
 AREA-AVERAGED Fm(INCH/HR) = 0.06  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.16  
 EFFECTIVE STREAM AREA(ACRES) = 13.51  
 TOTAL STREAM AREA(ACRES) = 17.46  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 33.26

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 72.10 TO NODE 73.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 274.00  
 ELEVATION DATA: UPSTREAM(FEET) = 147.21 DOWNSTREAM(FEET) = 146.38

Tc = K\*(LENGTH\*\* 3.00)/(ELEVATION CHANGE]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.156  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.870  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.42	0.40	0.100	32	9.16

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 1.07  
 TOTAL AREA(ACRES) = 0.42 PEAK FLOW RATE(CFS) = 1.07

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 73.00 TO NODE 73.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.16  
 RAINFALL INTENSITY(INCH/HR) = 2.87  
 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 0.42  
 TOTAL STREAM AREA(ACRES) = 0.42

PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.07

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	28.79	7.51	3.214	0.40( 0.06)	0.15	8.2	70.10
1	29.84	8.24	3.049	0.40( 0.06)	0.15	9.0	68.00
1	30.71	8.93	2.911	0.40( 0.06)	0.15	9.7	65.10
1	30.79	8.99	2.900	0.40( 0.06)	0.15	9.8	67.10
1	31.93	9.81	2.759	0.40( 0.06)	0.15	10.9	63.10
1	32.20	10.03	2.724	0.40( 0.06)	0.15	11.2	68.10
1	33.21	11.92	2.468	0.40( 0.06)	0.16	13.1	64.10
1	33.21	11.92	2.467	0.40( 0.06)	0.16	13.1	66.10
1	33.26	12.49	2.402	0.40( 0.06)	0.16	13.5	62.10
1	32.66	15.09	2.156	0.40( 0.06)	0.15	15.3	61.00
1	29.68	21.54	1.758	0.40( 0.06)	0.15	17.5	71.10
2	1.07	9.16	2.870	0.40( 0.04)	0.10	0.4	72.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	29.78	7.51	3.214	0.40( 0.06)	0.15	8.5	70.10
2	30.87	8.24	3.049	0.40( 0.06)	0.15	9.4	68.00
3	31.77	8.93	2.911	0.40( 0.06)	0.15	10.2	65.10
4	31.86	8.99	2.900	0.40( 0.06)	0.15	10.2	67.10
5	32.09	9.16	2.870	0.40( 0.06)	0.15	10.5	72.10
6	32.96	9.81	2.759	0.40( 0.06)	0.15	11.3	63.10
7	33.21	10.03	2.724	0.40( 0.06)	0.15	11.6	68.10
8	34.13	11.92	2.468	0.40( 0.06)	0.15	13.5	64.10
9	34.13	11.92	2.467	0.40( 0.06)	0.15	13.5	66.10
10	34.15	12.49	2.402	0.40( 0.06)	0.15	13.9	62.10
11	33.46	15.09	2.156	0.40( 0.06)	0.15	15.7	61.00
12	30.33	21.54	1.758	0.40( 0.06)	0.15	17.9	71.10

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 34.15 Tc(MIN.) = 12.49  
 EFFECTIVE AREA(ACRES) = 13.93 AREA-AVERAGED Fm(INCH/HR) = 0.06  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.15  
 TOTAL AREA(ACRES) = 17.9  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 73.00 = 2046.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 73.00 TO NODE 95.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 140.82 DOWNSTREAM(FEET) = 137.00  
 FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 14.03  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 34.15



PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 12.63  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 95.00 = 2161.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 95.00 TO NODE 95.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

-----  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.63  
 RAINFALL INTENSITY(INCH/HR) = 2.39  
 AREA-AVERAGED Fm(INCH/HR) = 0.06  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.15  
 EFFECTIVE STREAM AREA(ACRES) = 13.93  
 TOTAL STREAM AREA(ACRES) = 17.88  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 34.15

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 91.00 TO NODE 92.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

-----  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00  
 ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 151.50

Tc = K\*((LENGTH\*\* 3.00)/(ELEVATION CHANGE)\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.265  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.044  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN	(MIN.)
APARTMENTS	A	1.27	0.40	0.200	32	8.26

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA RUNOFF(CFS) = 3.39  
 TOTAL AREA(ACRES) = 1.27 PEAK FLOW RATE(CFS) = 3.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 92.00 TO NODE 93.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

-----  
 ELEVATION DATA: UPSTREAM(FEET) = 151.50 DOWNSTREAM(FEET) = 149.10  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 256.00 CHANNEL SLOPE = 0.0094  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.766  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
APARTMENTS	A	2.19	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.03  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.84  
 AVERAGE FLOW DEPTH(FEET) = 0.18 TRAVEL TIME(MIN.) = 1.50  
 Tc(MIN.) = 9.77  
 SUBAREA AREA(ACRES) = 2.19 SUBAREA RUNOFF(CFS) = 5.29  
 EFFECTIVE AREA(ACRES) = 3.46 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 8.36

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 3.14  
 LONGEST FLOWPATH FROM NODE 91.00 TO NODE 93.00 = 556.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 93.00 TO NODE 94.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

-----  
 ELEVATION DATA: UPSTREAM(FEET) = 149.10 DOWNSTREAM(FEET) = 148.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 180.00 CHANNEL SLOPE = 0.0061  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.610  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
APARTMENTS	A	1.70	0.40	0.200	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.30  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.88  
 AVERAGE FLOW DEPTH(FEET) = 0.28 TRAVEL TIME(MIN.) = 1.04  
 Tc(MIN.) = 10.81  
 SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 3.87  
 EFFECTIVE AREA(ACRES) = 5.16 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 11.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.30 FLOW VELOCITY(FEET/SEC.) = 3.01  
 LONGEST FLOWPATH FROM NODE 91.00 TO NODE 94.00 = 736.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 94.00 TO NODE 95.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

-----  
 ELEVATION DATA: UPSTREAM(FEET) = 148.00 DOWNSTREAM(FEET) = 137.00  
 FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.54  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 11.75  
 PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 10.95  
 LONGEST FLOWPATH FROM NODE 91.00 TO NODE 95.00 = 866.00 FEET.

13 38.15 21.68 1.751 0.40( 0.06) 0.16 23.0 71.10

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 45.34 Tc(MIN.) = 10.95  
 EFFECTIVE AREA(ACRES) = 17.54 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.17  
 TOTAL AREA(ACRES) = 23.0  
 LONGEST FLOWPATH FROM NODE 61.00 TO NODE 95.00 = 2161.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 95.00 TO NODE 95.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

-----  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.95  
 RAINFALL INTENSITY(INCH/HR) = 2.59  
 AREA-AVERAGED Fm(INCH/HR) = 0.08  
 AREA-AVERAGED Fp(INCH/HR) = 0.40  
 AREA-AVERAGED Ap = 0.20  
 EFFECTIVE STREAM AREA(ACRES) = 5.16  
 TOTAL STREAM AREA(ACRES) = 5.16  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.75

-----  
 END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 23.0 TC(MIN.) = 10.95  
 EFFECTIVE AREA(ACRES) = 17.54 AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.167  
 PEAK FLOW RATE(CFS) = 45.34

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	29.78	7.65	3.181	0.40( 0.06)	0.15	8.5	70.10
1	30.87	8.38	3.020	0.40( 0.06)	0.15	9.4	68.00
1	31.77	9.07	2.886	0.40( 0.06)	0.15	10.2	65.10
1	31.86	9.13	2.875	0.40( 0.06)	0.15	10.2	67.10
1	32.09	9.29	2.846	0.40( 0.06)	0.15	10.5	72.10
1	32.96	9.95	2.737	0.40( 0.06)	0.15	11.3	63.10
1	33.21	10.17	2.703	0.40( 0.06)	0.15	11.6	68.10
1	34.13	12.05	2.452	0.40( 0.06)	0.15	13.5	64.10
1	34.13	12.06	2.451	0.40( 0.06)	0.15	13.5	66.10
1	34.15	12.63	2.387	0.40( 0.06)	0.15	13.9	62.10
1	33.46	15.22	2.145	0.40( 0.06)	0.15	15.7	61.00
1	30.33	21.68	1.751	0.40( 0.06)	0.15	17.9	71.10
2	11.75	10.95	2.591	0.40( 0.08)	0.20	5.2	91.00

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	39.92	7.65	3.181	0.40( 0.07)	0.16	12.1	70.10
2	41.39	8.38	3.020	0.40( 0.07)	0.16	13.3	68.00
3	42.64	9.07	2.886	0.40( 0.07)	0.16	14.4	65.10
4	42.76	9.13	2.875	0.40( 0.07)	0.16	14.5	67.10
5	43.07	9.29	2.846	0.40( 0.07)	0.16	14.8	72.10
6	44.25	9.95	2.737	0.40( 0.07)	0.17	16.0	63.10
7	44.61	10.17	2.703	0.40( 0.07)	0.17	16.4	68.10
8	45.34	10.95	2.591	0.40( 0.07)	0.17	17.5	91.00
9	45.23	12.05	2.452	0.40( 0.07)	0.17	18.6	64.10
10	45.23	12.06	2.451	0.40( 0.07)	0.17	18.6	66.10
11	44.95	12.63	2.387	0.40( 0.07)	0.17	19.1	62.10
12	43.13	15.22	2.145	0.40( 0.07)	0.16	20.8	61.00
13	38.15	21.68	1.751	0.40( 0.06)	0.16	23.0	71.10

-----  
 END OF RATIONAL METHOD ANALYSIS

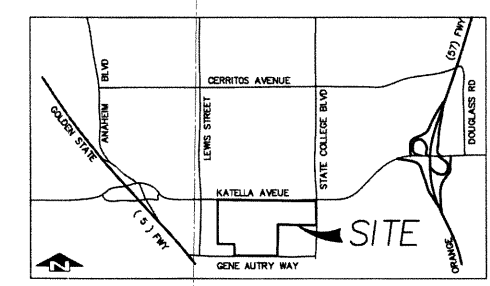
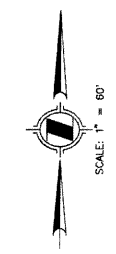
RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	39.92	7.65	3.181	0.40( 0.07)	0.16	12.1	70.10
2	41.39	8.38	3.020	0.40( 0.07)	0.16	13.3	68.00
3	42.64	9.07	2.886	0.40( 0.07)	0.16	14.4	65.10
4	42.76	9.13	2.875	0.40( 0.07)	0.16	14.5	67.10
5	43.07	9.29	2.846	0.40( 0.07)	0.16	14.8	72.10
6	44.25	9.95	2.737	0.40( 0.07)	0.17	16.0	63.10
7	44.61	10.17	2.703	0.40( 0.07)	0.17	16.4	68.10
8	45.34	10.95	2.591	0.40( 0.07)	0.17	17.5	91.00
9	45.23	12.05	2.452	0.40( 0.07)	0.17	18.6	64.10
10	45.23	12.06	2.451	0.40( 0.07)	0.17	18.6	66.10
11	44.95	12.63	2.387	0.40( 0.07)	0.17	19.1	62.10
12	43.13	15.22	2.145	0.40( 0.07)	0.16	20.8	61.00

**LEGEND**

- MAJOR DRAINAGE BOUNDARY
- MINOR DRAINAGE BOUNDARY
- NODE NUMBER
- AREA DESIGNATION
- AREA ACREAGE (IN ACRES)
- PEAK FLOW RATE
- TIME OF CONCENTRATION
- PEAK CONFLUENCE FLOW RATE
- TIME OF CONCENTRATION
- PROPOSED STORM DRAIN
- SOIL GROUP



**HYDROLOGY STUDY  
FOR A-TOWN  
TRACTS 17703 & 16859  
PROPOSED CONDITION**

PREPARED BY:  
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